

DRAFT ANNUAL COMPLIANCE REPORT

**Instream Flow Agreement
for the
Cedar River**

Cedar River Watershed Habitat Conservation Plan Year 24:
January 1 through December 31, 2024,
Including Summaries for HCP Years 1-24

Prepared by



City of Seattle

Seattle Public Utilities
and
Seattle City Light

April, 2024

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Acknowledgements

In 2024, Cedar River Instream Flow Commission (IFC) members devoted substantial time and effort to help manage water resources in the Cedar River Basin. IFC members also helped guide the development and implementation of supplemental biological studies and other technical analyses that continue to inform their management recommendations. The IFC members are, herein recognized for their continued commitment to effectively manage water resources in the Cedar River Basin and provide beneficial conditions for instream resources.

Organizational membership and representation are as follows:

Voting Organizations:

- National Marine Fisheries Service
 - Temporarily absent due to staffing issues
- United States Fish and Wildlife Service
 - Jeff Garnett
- Washington Department of Fish and Wildlife
 - Peggy Miller
- Washington Department of Ecology
 - Buck Smith
- Muckleshoot Indian Tribe
 - Eric Warner
- City of Seattle
 - Paul Faulds – Seattle Public Utilities
 - Karl Burton – Seattle Public Utilities
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 - Leska Fore– Seattle City Light

Non-Voting Organizations:

- Army Corps of Engineers
 - Kyle Comanor
- WRIA 8
 - Mary Ramirez

In addition, it takes many people in an organization to translate good intentions into successful operations. Providing beneficial conditions for fish and other instream resources in the Cedar River is a 24-hour, 365-day a year responsibility.

Special thanks go to staff from:

- SCL Cedar Falls Headworks
- SPU Water Supply and Treatment (Landsburg Operators and Control Center)
- SPU Watershed Management Division
- SPU Water Resources Section

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1. Introduction

The City of Seattle (“City”) influences river flows in the Cedar River through its water supply and hydroelectric operations within the municipal watershed. Water from the Cedar River is used by approximately two-thirds of the City's 1.6 million customers in King and Snohomish Counties. The objective of the Cedar River Instream Flow Agreement (IFA), one of several agreements that establish the provisions of the Cedar River Watershed Habitat Conservation Plan (HCP), is to provide beneficial conditions for instream resources, while preserving Seattle’s water supply and power generation capabilities.

The IFA establishes an interagency body, the Cedar River Instream Flow Oversight Commission (IFC) to assist the City in carrying out its river management responsibilities. The IFC was first convened in July 2000, and has met, on average, six to ten times a year since then. Meetings are chaired by Seattle Public Utilities (SPU).

1.1 Purpose of Report

SPU and Seattle City Light (SCL), on behalf of the City, present this report to the Commission as documentation of compliance with flow requirements established in the IFA. Section D.3 (a) of the IFA stipulates that an annual compliance report be submitted to the IFC. This report covers the period from January 1, 2024 through December 31, 2024. The report also summarizes compliance results for HCP years 1-24.

1.2 Highlights in 2024:

- Stream flows remained above the normal guaranteed levels at all times in 2024. All required supplemental stream flows were provided during the year.
- In 2024, there were two downramping exceedances at the U.S. Geological Survey (USGS) Gage 12117600 below Landsburg Diversion (see section 5.2.1).
- All downramping and minimum flow requirements below Masonry Dam (recorded at USGS gage 12116400) were met in 2024. Similarly, all downramping requirements below the Cedar Falls Powerhouse were met (recorded at USGS gage 12116500) were met with the exception of one downramping event on June 10, 2024 when downramping began two hours before the end of the day due to operator error.
- Construction of the new switchyard for the Cedar Falls Powerhouse began in mid-2023. A switchyard is a critical component of an electrical power system that serves as the connection point between the power plant and the transmission grid. Both Generators 5 and 6 were shut down on June 5, 2023. After construction was completed, generators were returned to operation on December 16, 2024.
- As in previous years, some minor, short-term fluctuations in flow and water surface elevation were identified below the Cedar Falls Powerhouse at USGS gage 12116500. Additional analysis of these occurrences found that small changes in flow are associated with turbines that drift from their set point during normal operations. Although the turbines are set to generate a specific amount of power, they fluctuate slightly which

can result in measurable changes in river flow. Fluctuations are more evident at lower flows, but generally last for less than an hour.

- The average annual Cedar River daily diversion for calendar year 2024 was 79.6 MGD.
- There were no flow events that exceeded the redd scour threshold of 2,200 cfs in the Cedar River (USGS Gage 12119000, Renton) in 2024. The highest flow recorded at the Renton Gage was 1930 cfs on January 28th.
- Spring redd surveys performed by SPU and WDFW documented seven steelhead redds and 24 trout redds in the mainstem Cedar River. The firm summer supplemental block of water was allocated and all observed redds were protected against dewatering throughout incubation and emergence.

2. Measuring Points

Flow and downramping compliance is measured at several locations throughout the Cedar River Watershed including:

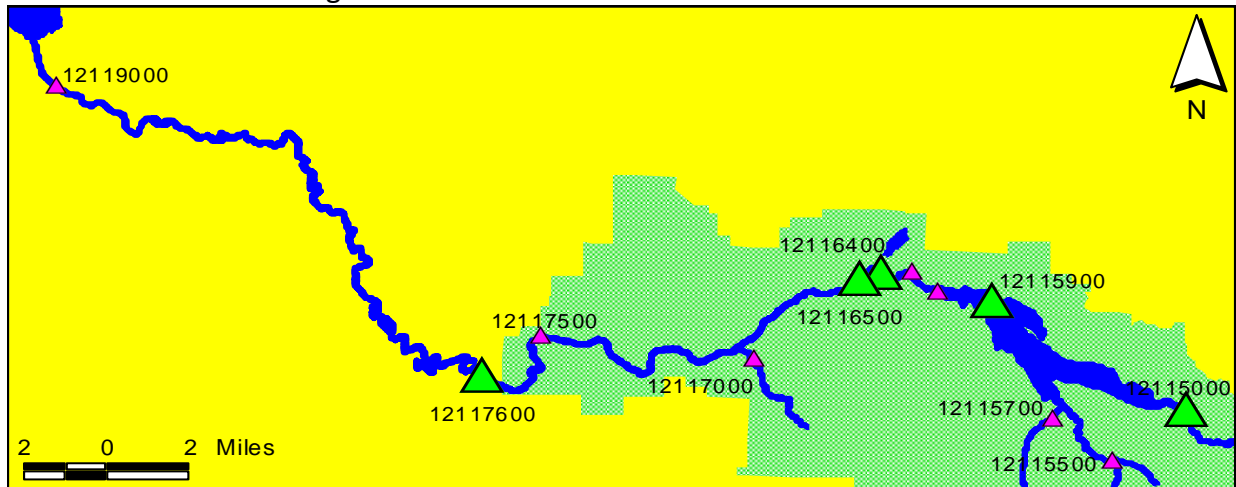


Figure 2.1. Map of Cedar River from Chester Morse Reservoir to Lake Washington showing flow measurement points for IFA.

USGS Gaging Station 12117500 – Cedar River below Diversion near Landsburg, Washington. Located at River Mile 20.4, this gage measures regulated stream flow downstream of Landsburg Diversion Dam. This is the measuring point for flows and downramping rates immediately below the Landsburg Diversion Dam, as required in Section B and sub-section C.2.c in the IFA.

Seattle Public Utilities Diversion Just Above 12117600 – Cedar River at the Diversion Dam near Landsburg, Washington. Located at River Mile 21.9, this measures the volume of water (in millions of gallons per day) diverted for municipal use and is monitored at the Landsburg Diversion Dam Facility.

USGS Gaging Station 12116500 – Cedar River at Cedar Falls, Washington. Located at River Mile 33.2, immediately below the Cedar Falls Powerhouse, this gage measures regulated stream flow downstream of the Cedar Falls Powerhouse. This is the measuring point for downramping rates immediately below the Powerhouse at Cedar Falls, as required in sub-section C.2.b in the IFA.

USGS Gaging Station 12116400 – Cedar River at Powerhouse at Cedar Falls, Washington. Located at River Mile 33.7, this gage is immediately upstream of the Cedar Falls Powerhouse and measures regulated stream flow downstream of Masonry Dam. This is the measuring point for flows and downramping rates immediately above the Cedar Falls Powerhouse, as required in sub-section C.1.a in the IFA. (Note: Date of installation Oct. 1, 2001).

USGS Gaging Station 12115900 – Chester Morse Reservoir at Cedar Falls, Washington. This gage located at the Overflow Dike at River Mile 37.2 and measures water surface elevation of Chester Morse Reservoir. This is the measuring point for determining reservoir elevation, as required in sub-sections B.7.b. (1) and B.8.c. (1).

USGS Gaging Station 12115000 – Cedar River near Cedar Falls, Washington. This gage located at River Mile 43.5 and measures unregulated inflows to Chester Morse Reservoir. This is the measuring point for determining reservoir inflows, as required in sub-sections B.7.b. (2), B.7.b. (3), and B.8.c. (2), and serves as an index for total reservoir inflow.

3. Instream Flows Below Landsburg Diversion Dam

In accordance with the IFA Section B.1.a, the City has two types of commitments, minimum instream flows and supplemental instream flows:

“consist of two types of commitments by the City. The minimum instream flows or volumes, as described in sub-sections B.2., B.4., B.6., B.7., and B.8., represent requirements of the City and are referred to as “firm” flows or volumes, subject to the specific conditions and procedures set forth therein. Additional flows or volumes provided to supplement minimum flows, as described in sub-sections B.3. and B.5., represent goals of the City and are referred to as “non-firm” flows or volumes, subject to the specific conditions and procedures set forth therein.”

On June 3, 2009, the Cedar River Habitat Conservation Plan Oversight Committee established interim weekly adjustments in the critical, normal, and supplemental flow schedules to compensate for hydrologic alterations of the Walsh Lake Ditch that occurred as a result of the January 2009 flood event (see Appendix 1). During this event, a landslide triggered a failure of the Walsh Ditch which resulted in the flow in Walsh Creek (the outlet from Walsh Lake) being reestablished in its original natural pathway flowing into Rock Creek and then to the Cedar River upstream of Landsburg Dam and upstream of the nearby instream flow compliance point at USGS Gage 12117600, (Cedar River Below Diversion Near Landsburg). Prior to this event, the flow from Walsh Creek was delivered via the Walsh Lake Ditch directly to the Cedar River approximately ½ mile downstream of the compliance point at USGS Gage 12117600. As long as Walsh Creek continues to flow in its current pathway to Rock Creek and the Cedar River upstream of the Landsburg Dam, SPU will comply with the revised instream flow schedule. SPU will also continue to monitor actual flows in Walsh Creek in an effort to further evaluate the degree to which the interim adjustments appropriately reflect actual Walsh Creek flow trends.

3.1 Minimum Instream Flows Below Landsburg Dam

Compliance with minimum flow requirements is assessed at one monitoring location in the Cedar River below Landsburg: USGS Gage 12117600 - Cedar River below Diversion near Landsburg.

3.1.1 Requirements

Required minimum flows are specified in Sections B.2.a and B.2.b in the IFA and the minimum flow requirement schedule is specified in Section B.2.c:

“The City shall provide the minimum instream flows as set forth in sub-section B.2.c. Unless otherwise specified, the flows listed in sub-section B.2.c and elsewhere in this Agreement represent flow rates measured as “provisional real-time” data at the existing USGS Gage number 12117600, located below Landsburg Diversion Dam at river mile 20.4. Normal minimum flows are defined as the minimum instream flow rates that the City will provide below Landsburg Diversion Dam except when all of the conditions and procedures specified in Section B.8. are met, in which case the City, in consultation with the Commission, may provide critical minimum flows.”

3.1.2 Compliance

During the 2024 reporting period, the project was in compliance with the IFA guaranteed minimum flows at USGS Gage 12117600. See Figure 8.1 and Tables 8.1 and 8.2.

For long-term tracking purposes, stream flows have remained at or above guaranteed normal minimum levels at all times in HCP Years 1 through 24, with the exception of an event in 2023 when flows dropped slightly below the minimum flow, and a 7-day period in October of 2015 when flows were managed at levels between low normal minimums and critical flows due to a significant statewide drought. The minimum flow violation in 2023 occurred on November 11th between 9:30 am and 10:15 am when flows dropped to 278 cfs at the 12117600 gage. The minimum flow for November 11th is 279 cfs. The 2015 event was approved by the IFC.

3.2 Non-Firm Supplemental Flow in Late Winter and Early Spring for Sockeye Outmigration

3.2.1 Goals

Flow requirements are specified in Section B.3.a in the IFA:

“Between February 11 and April 14, the City will, as a goal, expect to supplement the normal minimum instream flows listed in sub-section B.2.c. by 105 cfs at least 70% of the time throughout said period in any year in which normal flows are in effect throughout said period.”

3.2.2 Compliance

The City met and exceeded the goal in 2024 by providing more than 105 cfs of supplemental flow 92% of the days during the February 11 to April 14 supplemental period (59 of 64 days). See Table 3.2.1.

For long-term tracking, this goal has been met or exceeded in 22 of 24 years (Table 3.2.2.). The supplemental flow was not provided in 2001 and 2005, years in which the State of Washington declared statewide droughts.

Table 3.2.1 Supplemental flows for sockeye fry outmigration 2024.

Calendar Dates	Required Normal Minimum Instream Flows (cfs)	Minimum Instream Flows Plus Non-Firm Supplemental Flows (cfs)	Actual Recorded Mean Daily Flow (cfs)	Calendar Dates	Required Normal Minimum Instream Flows (cfs)	Minimum Instream Flows Plus Non-Firm Supplemental Flows (cfs)	Actual Recorded Mean Daily Flow (cfs)
11-Feb	273	378	425	15-Mar	273	378	391
12-Feb	273	378	465	16-Mar	273	378	393
13-Feb	273	378	453	17-Mar	273	378	394
14-Feb	273	378	460	18-Mar	273	378	395
15-Feb	273	378	443	19-Mar	273	378	397
16-Feb	273	378	445	20-Mar	273	378	394
17-Feb	273	378	445	21-Mar	273	378	432
18-Feb	273	378	429	22-Mar	273	378	507
19-Feb	273	378	410	23-Mar	273	378	542
20-Feb	273	378	416	24-Mar	273	378	446
21-Feb	273	378	421	25-Mar	273	378	424
22-Feb	273	378	433	26-Mar	273	378	463
23-Feb	273	378	487	27-Mar	273	378	529
24-Feb	273	378	481	28-Mar	273	378	534
25-Feb	273	378	566	29-Mar	273	378	513
26-Feb	273	378	630	30-Mar	273	378	497
27-Feb	273	378	624	31-Mar	273	378	483
28-Feb	273	378	668	1-Apr	273	378	472
29-Feb	273	378	776	2-Apr	273	378	459
1-Mar	273	378	728	3-Apr	273	378	428
2-Mar	273	378	707	4-Apr	273	378	406
3-Mar	273	378	691	5-Apr	273	378	396
4-Mar	273	378	688	6-Apr	273	378	393
5-Mar	273	378	667	7-Apr	273	378	399
6-Mar	273	378	652	8-Apr	273	378	395
7-Mar	273	378	642	9-Apr	273	378	389
8-Mar	273	378	633	10-Apr	273	378	326
9-Mar	273	378	556	11-Apr	273	378	304
10-Mar	273	378	453	12-Apr	273	378	305
11-Mar	273	378	449	13-Apr	273	378	322
12-Mar	273	378	484	14-Apr	273	378	315
13-Mar	273	378	425				
14-Mar	273	378	396				

Table 3.2.2 Percent of days by year that supplemental flows were provided for juvenile sockeye outmigration during the February 11 to April 14 period, 2000-2024.

Year	% of Feb.11 to April 14 Time Period with 105 cfs Supplemental Flow	Year	% of Feb.11 to April 14 Time Period with 105 cfs Supplemental Flow
2000	100	2013	100
2001	13	2014	100
2002	100	2015	71
2003	90.5	2016	100
2004	100	2017	100
2005	24	2018	100
2006	100	2019	83
2007	100	2020	97
2008	100	2021	100
2009	100	2022	100
2010	92	2023	83
2011	92	2024	92
2012	100		

3.2.3 Hydrologic Summaries for HCP Years When Supplemental Flows for Juvenile Sockeye Outmigration Were Not Met for 70% of the Feb 11 – April 14 Period.

2001: Supplemental flows for sockeye outmigration were provided only 13% of the 2001 supplemental outmigration flow time period. The underlying consideration that prevented the City from meeting the supplemental flow goal of 70% for the supplementation period was the unprecedented drought conditions that prevailed in the region from November through mid-March. Entering the February 11 to April 14 period, all indicators showed reason for concern and resulted in SPU's conservative treatment for the water held in storage in Chester Morse Reservoir as well as the South Fork Tolt Reservoir. Extremely low winter precipitation (the lowest in 70 years) and associated low reservoir inflows, poor snowpack, and low reservoir contents were observed during this period. SPU's SEAFM forecast model was showing a significant likelihood of not refilling the mountain reservoirs before summer.

Precipitation at Chester Morse Reservoir was about 30 inches for October, November, December, January and February combined; normal precipitation is over 62 inches in those months. The four-month period of November through February had the lowest precipitation for the same four-month period ever recorded in the Cedar Watershed. Inflows to the City's reservoirs were above normal until late October, but by late November and through December they were near record low levels. From October 1 to January 1, Chester Morse Reservoir went from being five feet above normal, to ten feet below normal and the South Fork Tolt Reservoir went from being near normal to 12 feet below normal. Chester Morse Reservoir approached its lowest elevation of 1540 feet in late November and then held relatively steady until the last

week of December. Typically, Chester Morse Reservoir is in flood management mode in November and December and the reservoir surface elevation is above 1550 feet. In November 2000, South Fork Tolt Reservoir reached elevation 1742 feet. The drought weather pattern changed temporarily on December 25th and inflows rebounded to normal levels, although snowpack did not build significantly.

In late December and early January, Chester Morse Reservoir gradually rose about eight feet and the South Fork Tolt Reservoir rose about two feet. Shortly after January 1, 2001, the weather turned unusually dry again, and unregulated streamflows and inflows to the City's reservoirs returned to very low levels throughout January 2001. Storms in early February improved streamflows for a time, but extremely dry conditions returned and persisted until mid-March 2001. Significant storm events in mid-March improved the water supply outlook somewhat. Total March and April precipitation in the Cedar River Watershed was about 21.2 inches; in an average March and April, precipitation is about 18.5 inches. However, the improvement was not considered adequate to ensure refill and the IFC agreed to forego flow supplementation for the remainder of the Feb. 11 to April 14 time period.

2005: Supplemental flows for sockeye outmigration were provided for 24% of the Supplemental Outmigration Flow time period. The underlying consideration that prevented the City from meeting the supplemental flow goal of 70% for the supplementation period was the extremely low snowpack and exceptionally dry conditions that prevailed in the region from January through March. Based on worsening snowpack and record low inflows the City reduced the supplemental flow to normal flow levels on February 26. On March 4 the City issued a news release stating Seattle Public Utilities was cautious about the water supply conditions and that the recent dry conditions led to a reduction in supplemental flows. On March 10, Governor Christine Gregoire authorized the Department of Ecology to declare a statewide drought emergency, based on the extremely low snowpack in the mountains and record-low flows. On March 16 Seattle Mayor Greg Nickels invoked the Advisory Stage of Seattle's Water Shortage Contingency Plan. The following is a brief synopsis of the drought through April: Precipitation at Chester Morse Reservoir was about 29 inches for January through April combined; normal precipitation is over 42 inches. Following the low rainfall pattern, eight-week moving average inflows to City reservoirs were above normal until late January, but by early March they were below the alert phase index. From March 1 to April 8, Chester Morse Reservoir was below the generalized rule curve. Chester Morse Reservoir approached its lowest 2005 elevation in late March. The March 1 statewide Natural Resources Conservation Service (NRCS) Snow Telemetry (SNOTEL) Snow Water Equivalent (SWE) readings were 26% of average. NRCS reported the Central Puget Basin SWE was 20% of average.

The IFC were aware of the developing difficult hydrologic conditions and took an active role in the development and implementation of a water management strategy to manage impacts to instream resources and municipal water users. General consensus was reached that both instream resources and municipal water users could be potentially impacted by the developing conditions and that interest of both needed to be considered in developing potential management responses. The Commission agreed that early proactive steps were necessary to

reduce the risk of major impacts later in the year. The first step in a coordinated management response was the suspension of supplemental spring stream flows coupled with a strong SPU public messaging campaign and SPU’s formal implementation of the Advisory Stage of Seattle’s Water Shortage Contingency Plan to encourage municipal water users to conserve water. Due in part to these early actions, stream flows were never reduced to critical levels and remained at or above normal guaranteed levels for the remainder of the year.

3.3 Firm Block of Water in Early Summer to Supplement Normal Minimum Flows for Steelhead Incubation

3.3.1 Requirements

Flow requirements are specified in Section B.4 in the IFA:

“Between June 17 and August 4, in addition to the normal minimum flows listed in subsection B.2.c., the City shall provide such supplemental flow volumes as the Commission may direct, provided that the total volume of such supplemental flows shall not exceed 2500 acre-feet of water, and that other procedures and conditions in this sub-section B.4. are met.”

3.3.2 Compliance

In 2024, the City provided the Firm Block as prescribed by the Commission. See Table 3.3.1 and Figure 8.1. The firm block was distributed as late in the period as allowed by the IFA.

Table 3.3.1 Minimum flows and minimum flows plus summer supplemental firm block by week, June 17 – August 4.

Calendar Dates	Required Minimum Instream Flows, cfs	Required Minimum Flow plus 2022 Summer Supplemental Firm Block, cfs
June 17 – July 30	231	231
July 1 – July 7	174	174
July 8 – July 18	109	164
July 19 – July 23	84	134
July 24 – July 28	84	118
Jul 29 – Aug 1	84	108
Aug 2 – Aug 4	83	95

For long-term tracking, this goal has been met or exceeded in all 24 HCP years.

3.4 Non-Firm Block of Water in Early Summer to Supplement Normal Minimum Flows for Steelhead Incubation

3.4.1 Goals

Flow requirements are specified in Section B.5 in the IFA:

“Between June 17 and August 4, in addition to the normal minimum flows listed in sub-section B.2.c, and the “firm block” described in sub-section B.4., the City will, as a goal and under the conditions set forth in this sub-section B.5., expect to further supplement normal minimum flows by 3500 acre-feet of “non-firm” water in 63% of all years.”

3.4.2 Compliance

The City did not offer the 3,500 Acre-Feet Supplemental Block in 2024. See Table 8.1 and Figure 8.1.

For long-term tracking purposes, SPU has offered the full non-firm block in 20 out of 24 years (83% with 2003, 2015, 2016 and 2024 being the exceptions). The Commission was offered but declined allocation of the block in two years (2004 and 2023). As described in the Instream Flow Agreement, the City received credit for allocating the non-firm supplemental block in 2004 and 2023 as part of the commitment to provide the non-firm block in 63% of HCP years

3.4.3 Hydrologic Conditions and Vulnerable Redd Summary for HCP Years when the 3,500 acre-foot Non-firm Supplemental Block of Water was not Offered by the City

2003 – Chester Morse Reservoir was at surface water elevation 1561.5 feet in early June. Very small amounts of snow remained in the Cedar Basin and the expected elevation without additional rain was 1562 feet. The month of May had only 66% of its normal rainfall and April was also relatively dry. The watershed was considered very dry at the time of the non-firm block decision with most local and inflow streams registering near the 20-percentile dry condition. The snowpack was poor in early June with approximately 65% of normal SWE. The winter also had low rain volume at lower elevations after a very dry summer and fall the previous year. The Chester Morse and South Fork Tolt reservoirs were relatively full in 2003 but continued dryness caused the reservoirs to drop faster than normal. In June, SPU was not anticipating any problems that would require water curtailments. In 2003, there were 12 observed steelhead redds in the Cedar River, none of which needed supplemental flow above summer minimums to remain submerged through the end of emergence. The City decided not to offer the 3,500 acre-foot of supplemental water.

2015 - Precipitation levels in May of 2015 were the driest on record for that month. April also had below average precipitation. The extended forecast in June was for very dry weather. Cedar River Municipal Watershed flow measurements indicated that tributaries to Chester Morse Reservoir were flowing at levels typically observed in late July or August. Chester Morse Reservoir elevation in early June was 1561.6 feet and dropping ¼ foot a day with record low inflows. Snowmelt was complete in the first week of May. Demand was substantially higher than 2014 and SPU sent out a customer mailer dedicated to urging wise water use. Due to the

lack of snow, all Hydrocomp Forecast and Analysis Model (HFAM) hydrologic model runs assumed that the 3,500 acre-foot non-firm supplemental block of water had not been allocated. HFAM is a continuous simulation hydrologic model that is designed specifically for the South Fork Tolt and Cedar River Watersheds. The snowpack in the Central Puget Sound Basin was 0% of normal and the 8-week average inflow was below the alert phase, which is unusual for that time of year.

Four steelhead redds and 15 trout redds were observed in the Cedar River in 2015. One steelhead redd was vulnerable to partial dewatering at flows below 255 cfs. No trout redds were vulnerable to dewatering. The vulnerable steelhead redd needed 24 cfs of voluntary flow supplementation from June 10 to June 14 to keep it submerged through the predicted end of emergence. No supplemental water was needed to keep all remaining incubating redds fully watered throughout the supplemental flow allocation period (June 17 – August 4). SPU did not offer the non-firm supplemental block of water in 2015. The allocation plan for the 2,500 acre-foot firm block was allocated to load the available water as late into the summer as allowed to provide maximum benefits to instream resources.

2016 - Snowpack in 2016 was lower than average and snowmelt occurred approximately one month earlier than normal. Precipitation in April and May was below average. An early refill strategy for Chester Morse Reservoir was implemented and refill occurred during the second week in May. Chester Morse Reservoir was still full on June 1. The South Fork Tolt Watershed had lower than average snowpack and the reservoir did not reach the refill target in 2016. The early refill strategy and a substantial rain event in early June allowed combined reservoir storage to be above normal in early June. Due to the South Fork Tolt Reservoir elevation being lower than normal, SPU relied more heavily on Cedar River water with 70% of water supply originating from the Cedar Basin. Inflows were below the switching criteria for critical flows but the reservoir elevation was well above switching criteria level. HFAM model runs indicated that SPU would need to mobilize its two floating pump plants to access water stored below elevation 1538 feet in the Chester Morse Reservoir if summer precipitation was equivalent to a 98-percentile dry year in the historic weather record. The floating pump plants can be used to pump the lower elevation water over the natural outlet in the reservoir and into the river, thereby augmenting both instream flows and water availability for customer use. This assumed that the 3,500 acre-foot non-firm supplemental block was not allocated and SPU provided high normal flows in the fall. HFAM model runs indicated that Chester Morse Reservoir elevation could reach as low as 1540 feet and South Fork Tolt Reservoir elevation could reach 1716 feet. The long-term weather forecast was calling for normal precipitation and above normal temperatures.

Redd surveys between early March and late May documented six steelhead redds and 24 trout redds in the Cedar River. All trout redds were fully protected against dewatering by the HCP minimum flow regime without allocation of supplemental water. Of the six identified steelhead redds, only one redd required additional water above summer HCP minimum flows for protection against redd dewatering. The vulnerable redd required 95 cfs to maintain redd submergence until emergence was complete on or before July 24. Therefore, given the very low inflows and dry hydrologic conditions in both watersheds, the forecast for warmer than normal summer conditions, and the very small amount of water necessary to protect the vulnerable steelhead redd, SPU believed it was not prudent to allocate the summer non-firm block of supplemental water (3500 acre-feet) in 2016. The IFC agreed with the allocation plan in early June and the City provided adequate water to protect the vulnerable steelhead redd.

2024 - Snowpack in 2024 was well below average and there was no significant snow accumulation after mid-March. Precipitation in April and May was average but March was relatively dry with only approximately 60% of normal precipitation. An early refill strategy for Chester Morse Reservoir was implemented with a new refill target of 1565 feet. Refill occurred during the first week of June. The South Fork Tolt Watershed also had well below average snowpack. The South Fork Tolt Reservoir reached 1765 feet in early June. Inflows to both reservoirs were slightly above the switching criteria for critical flows. The long-term weather forecast was calling for dryer than normal in for precipitation and above normal temperatures.

Redd surveys between early March and late May documented seven steelhead redds and 24 trout redds in the Cedar River. All steelhead redds were fully protected against dewatering by the HCP minimum flow regime without allocation of supplemental water. Of the 24 identified trout redds, only one redd needed additional water above summer HCP minimum flows for protection against redd dewatering. The vulnerable redd required 159 cfs (USGS 12117600) to maintain redd submergence until emergence was complete on or before July 22nd when the minimum flow would be 84 cfs without supplementation. The vulnerable redd required less than 2,500 acre feet of water for full protection and SPU allocated the firm supplemental block accordingly. SPU decided not to allocate the summer non-firm block of supplemental water (3500 acre-feet) because it wasn't required for redd protection and because the City has met the non-firm block allocation for 83% of HCP years while the target for allocation is 63% of years. The IFC agreed with the summer supplemental water allocation plan in early June and the City provided the supplemental water to protect the vulnerable trout redd and provide benefits to other instream resources.

3.5 Higher Normal and Critical Minimum Flows in September for Sockeye and Chinook Spawning

3.5.1 Requirements

Flow requirements are specified in Section B.6 in the IFA:

“In any year in which the temporary flashboards, as they presently exist in the City’s Overflow Dike or may hereafter be reconstructed, are in place throughout the period of June 1 through September 30, the normal minimum flows listed in sub-section B.2.c. shall be increased by the amount of 38 cfs between September 15 and 22, and by the amount of 115 cfs between September 23 and 30, and the critical minimum flows shall be increased by the amount of 10 cfs through the period between September 1 and 15.”

3.5.2 Compliance

Temporary flashboards were in place throughout the period from June 1 through September 30, 2024, and the City provided the required additional flows. See Tables 3.5.1, 8.1 and Figure 8.1.

Table 3.5.1 Minimum flows when flashboards are in place September 16 – September 30.

Calendar Dates	Required Minimum Instream Flows, cfs	Minimum Instream Flows Plus High Normal Minimum Flows, cfs
Sep 16 - Sep 22, 2024	98	136
Sep 23 - Sep 30, 2024	98	214

For long-term tracking, high normal flows have been provided at all times during this period in HCP Years 1 through 24.

3.6 Two-Part Normal Minimum Flow Regime in the fall for Sockeye and Chinook Spawning

3.6.1 Requirements

Flow requirements are specified in Section B.7 in the IFA:

“Between October 8 and December 31, the City shall provide either high-normal minimum flows of 330 cfs or low-normal minimum flows of 275 cfs, except when flows are reduced to critical minimum flows under the terms of sub-section B.8. More specifically, the City, beginning on October 8, will meet the high-normal and low-normal flow regimes with the following long-term average frequencies assuming that the critical minimum flow regime will be in effect at a long-term average frequency of one of ten years:

(1) The City will follow the high-normal minimum flow regime in six of ten years, provided that it may switch down to low-normal in one of those years when actual or forecasted water availability conditions worsen significantly from those projected and understood at the time of the decision to provide high-normal minimum flows.

(2) *The City may follow the low-normal minimum flows in three of ten years, provided that it will switch up to high-normal at such time after October 8 if the City determines that improving conditions allow, or when criteria for high-normal are met, whichever comes first."*

3.6.2 Compliance

In early October 2024, the 15-day antecedent inflows to Chester Morse Reservoir were below the criteria of 32 cfs for providing high normal flows. Forecasts predicted that October would be dryer than normal. Low normal flows were provided for the period between October 8th and December 3rd. there were 8 days in that period when flows exceeded 330 cfs. In early December there was a significant rain event and high normal flows were provided between December 3rd and December 30th with the exception of when significant rain increased inflows and criteria for high normal were met. High normal flows were maintained until unusually low late November and early December precipitation levels prompted SPU to ask the IFC to reduce flows to low normal levels until significant precipitation occurred. The IFC approved the request and low normal flows were implemented between December 17th and 19th and again between December 21st and 23rd, when a storm provided sufficient rain volumes to return to high normal flows through December 30th. See Table 8.1 and Figure 8.1.

The City has exceeded the expected amount of time High Normal Flows were to be provided as outlined in the IFA (Actual 67% vs IFA Expected 60%). Low Normal Flows have been provided 28% of years and Critical Flows have been provided 4% of years. For long term tracking for provision of High Normal, Low Normal and Critical Flows by Week and by Number of Days. See Tables 3.6.1 and 3.6.2.

Table 3.6.1. Actual and expected high normal, low normal and critical flows by week, October 8 to December 30, 2024.

Week Period	Actual 2024	Expected % of time as per IFA			Actual % of time 2000-2024		
		High Flow	Low Flow	Critical Flow	High Flow	Low Flow	Critical Flow
Oct. 8 – Oct. 14	Low	60	30	10	74	26	0
Oct. 15 – Oct. 21	Low	60	30	10	81	19	0
Oct. 22 – Oct. 28	5 Low, 2 High	60	30	10	79	18	3
Oct. 29 – Nov. 4	5 Low, 2 High	50	40	10	86	13	1
Nov. 5 – Nov. 11	5 Low 2 High	55	35	10	91	9	0

Nov. 12 – Nov. 18	High	65	25	10	89	11	0
Nov. 19 – Nov. 25	High	65	25	10	92	8	0
Nov. 26 – Dec. 2	4 Low 3 High	70	20	10	92	8	0
Dec. 3 – Dec. 9	4 Low 3 High	75	15	10	93	7	0
Dec. 10 – Dec. 16	Low	75	15	10	95	5	0
Dec. 17 – Dec. 23	1 Low 6 High	80	10	10	92	8	0
Dec. 24 – Dec. 30	High	80	10	10	96	4	0

Table 3.6.2. Actual high normal, low normal and critical flows by number of days in week, October 8 to December 30, 2001 - 2024.

Week of Fall Supplemental Flow Period	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012
Oct 8 - Oct 14	High	High	3 Low, 4 High	High	High	High	High	High	Low	High	High	Low
Oct 15 - Oct 21	High	High	High	High	High	High	High	High	6 Low, 1 High	High	High	High
Oct 22 - Oct 28	High	Low	High	High	High	High	High	High	6 High, 1 Low	High	High	High
Oct 29 - Nov 4	High	Low	High	High	High	High	High	High	High	High	High	High
Nov 5 - Nov 11	High	Low	High	High	High	High	High	High	High	High	High	High
Nov 12 - Nov 18	High	Low	High	High	High	High	High	High	High	High	High	High
Nov 19 - Nov 25	High	Low	High	High	High	High	High	High	High	High	High	High
Nov 26 - Dec 2	High	Low	High	High	High	High	High	High	High	High	High	High
Dec 3 - Dec 9	High	Low	High	High	High	High	High	High	High	High	High	High
Dec 10 - Dec 16	High	5 Low, 2 High	High	High	High	High	High	High	High	High	High	High
Dec 17 - Dec 23	High	Low	High	High	High	High	High	High	High	High	High	High
Dec 24 - Dec 30	High	6 Low, 1 High	High	High	High	High	High	High	High	High	High	High
Week of Fall Supplemental Flow Period	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024
Oct 8 - Oct 14	High	High	Low	High	High	High	High	High	High	Low	6 Low, 1 high	Low
Oct 15 - Oct 21	High	High	Low	High	High	High	High	High	High	Low	5 Low, 2 high	Low
Oct 22 - Oct 28	High	High	2 Low, 5 Critical	High	High	High	High	High	High	Low	Low	Low
Oct 29 - Nov 4	High	High	2 Critical, 5 High	High	High	High	High	High	High	2 Low, 5 High	Low	5 Low, 2 high
Nov 5 - Nov 11	High	High	High	High	High	High	High	High	High	High	3 Low, 4 High	5 Low, 2 high
Nov 12 - Nov 18	High	High	High	High	High	High	High	High	High	High	Low	5 Low, 2 high
Nov 19 - Nov 25	High	High	High	High	High	High	High	High	High	High	Low	High
Nov 26 - Dec 2	High	High	High	High	High	High	High	High	High	High	6 Low, 1 High	High
Dec 3 - Dec 9	High	High	High	High	High	High	High	High	High	High	High	4 Low, 3 High
Dec 10 - Dec 16	High	High	High	High	High	High	High	High	High	High	High	4 Low, 3 High
Dec 17 - Dec 23	High	High	High	High	High	High	High	High	High	6 Low, 1 High	High	1 Low, 6 High
Dec 24 - Dec 30	High	High	High	High	High	High	High	High	High	High	1 Low, 6 High	High

3.7 Reductions to Critical Minimum Flows

3.7.1 Requirements

Required minimum flows are specified in Section B.8 in the IFA:

“This sub-section describes the circumstances under which the Parties agree that the City may switch to the minimum flow levels indicated in the column headed “Critical Flows” in the table which appears in sub-section B.2.c., until such time as those criteria may be modified pursuant to section E.4.”

3.7.2 Compliance

The City did not switch to the critical flow levels at any time during the 2024 reporting period. See Table 8.1 and Figure 8.1.

For long-term tracking purposes, stream flows have remained at or above guaranteed normal critical levels at all times in HCP Years 1 through 24, with the exception of a 7-day period in October of 2015 when flows were managed between low normal minimums and critical flow levels, as approved by the IFC. This exception is observed as if critical levels had been realized in 2015 (4% of HCP years).

3.7.3 Summary of 2015 Hydrologic Conditions Leading to Reduction of Flows to Levels Between Low Normal and Critical Flows

In 2015, snowpack was well below average and snowmelt in the Cedar River Municipal Watershed was complete by the first week of May. Precipitation levels in May were the driest on record for that month. April also had below average precipitation. Reservoir refill was moved up to May 1 and an additional one foot of water was stored compared to the normal refill elevation of 1563 feet. With very little snowmelt and a very dry spring, reservoir drawdown began a few weeks early. The extended forecast in June was for above average temperatures and very dry weather. In early June, Cedar River Municipal Watershed flow measurements indicated that tributaries to Chester Morse Reservoir were flowing at levels typically observed in late July or August. Chester Morse Reservoir elevation in early June was 1561.6 feet and dropping $\frac{1}{4}$ foot a day with record low inflows. Demand was higher than 2014 and SPU sent out a customer mailer dedicated to using water wisely. The 8-week average inflow was below the alert phase, which was unusual for early June. The month of June was the warmest and driest on record and many streams reached record low flows.

In July, there was a steep decline in the elevation of Chester Morse Reservoir. Unusually warm weather exacerbated normal reservoir decline by increasing water consumption. The May-June-July period was the driest on record for those three months combined. The 8-week moving average for inflows in July was below the alert phase and below the 5-percentile dry level. SPU implemented the use of their Seattle Wells from July to October to provide an additional 8 MGD of groundwater.

In early August, Chester Morse Reservoir elevation was slightly below 1550 feet and South Fork Tolt Reservoir elevation was approximately 1734 feet. Masonry Pool was split from the reservoir and SPU was drawing down Masonry Pool to limit leakage into the Cedar Moraine. Reservoir elevation was below the alert phase indicating SPU may need to consider plans to revert to a lower flow regime and floating pump plant mobilization. At 30 cfs, the 8-week moving average for reservoir inflows into Chester Morse was well below the alert phase. SPU invoked its Water Shortage Contingency Plan in late July and voluntary curtailment began in early August. August HFAM runs predicted a reservoir elevation of 1538 feet by the first week of October assuming precipitation was at 80 to 95-percentile dry, the City continued using the

wells, did not curtail water, and critical flows were not realized. SPU also used municipal pump stations in the distribution system to convey Cedar River water to some customers that are usually supplied water by the South Fork Tolt Reservoir.

By early September, the elevation of Chester Morse Reservoir was 1548.6 feet and the elevation of South Fork Tolt Reservoir was 1722 feet. Combined reservoir storage was well below the average for early September. HFAM model runs assumed low normal flows through October 8 and reduced flow scenarios thereafter in combination with 10% curtailment. The runs for 95-percentile dry and 98-percentile extremely dry showed that flows would need to be reduced to below low normal or to critical levels to ensure water supply and adequate flows for fish. Pump plants were mobilized and ready to pump to maintain low normal flows with a pumping capacity of 350 cfs.

By the end of September, Chester Morse Reservoir elevation was 1546.4 feet and Masonry Pool was drawn down to 1512 feet to limit seepage to the Cedar Moraine. The 8-week moving average for inflows was well below the inflow requirement of 37 cfs for moving to critical flows but the reservoir was above the 1540 feet elevation required to switch to critical flows. Normal flow levels had been provided throughout September. To provide high normal flows on October 8, the reservoir needs to be above 1541.5 feet and average inflows for the antecedent 30-day period and the antecedent 15-day period need to be greater than 31 cfs and 32 cfs, respectively. The South Fork Tolt Reservoir elevation was 1717 feet, which is below the elevation necessary to move to critical flows. After SPU invoked the voluntary curtailment process in the Water Shortage Contingency Plan in late July, regional water users conserved 14% when compared to projected water use. HFAM model run scenarios assumed continued use of Seattle's wells and water curtailment, low normal fall flows and 1 in 40 dry year, resulted in a predicted reservoir elevation of 1524 feet in first week of December. Model results that assumed a switch to critical flows on October 8 and one in 20-year dry conditions indicated that SPU would not need to operate the floating pump plants. Conditions remained dry and pump plants began pumping on October 18 to raise Masonry Pool elevation and provide an emergency source of water in case the pumps failed. Between elevations 1525 feet and 1530 feet, Masonry Pool can provide up to 2.5 days of water for instream flows. SPU followed the low normal flow regime until October 23 when the decision was made to drop to a minimum flow midway between low normal and critical flows. At the time, Chester Morse Reservoir was at elevation 1539.8 feet and South Fork Tolt Reservoir was at elevation 1713.8 feet. Inflows to both reservoirs were well below levels for switching to critical flows. For seven days in October, flows were at or slightly above critical flows. On October 31, an atmospheric river delivered over ten inches of rain to both basins and reservoir levels and stream flows improved substantially allowing SPU to provide high normal flows in the Cedar River for the remainder of the year.

4. Instream Flows Above Landsburg Diversion Dam

4.1 Flows between Cedar Falls Powerhouse and Masonry Dam

Compliance with minimum flow requirements is assessed at one monitoring location within the Cedar River Watershed: USGS Gage 12116400 - Cedar River at Powerhouse near Cedar Falls.

4.1.1 Requirements

Required minimum flows are specified in Section C.1.a in the IFA:

“After construction of a fish ladder at Landsburg Diversion Dam and subsequent upstream passage of selected species of anadromous fish, the City will provide a minimum flow of 30 cfs on a continuous basis to protect rearing habitat in the Cedar River “Canyon Reach,” measured by a new USGS stream gage to be installed near river mile 33.7 and funded by the City”

The fish ladder was completed and operational September 1, 2003. The first anadromous fish passed above Landsburg Diversion Dam on September 19, 2003, which marks the date the City started to provide a minimum flow of 30 cfs on a continuous basis in the Cedar River “Canyon Reach below USGS Gage 12116400 (see map, page 7).”

4.1.2 Compliance

During the 2024 reporting period, the project was in compliance with the IFA for minimum flow at USGS Gage 12116400. See Table 8.4 and Figure 8.6.

For long-term tracking purposes, stream flows at the USGS Gage 12116400 location have remained above 30 cfs at all times after the implementation of the 30 cfs minimum flow requirement in 2003.

5. Downramping below City Facilities

5.1 Downramping below Landsburg Diversion Dam

5.1.1 Requirements

Required downramping rates below Landsburg Dam are specified in Section C.2.c in the IFA:

“(1) General

(a) The downramping rates and procedures set forth in this sub-section C.2.c. will become effective not later than the end of HCP Year 2 and will apply to operations at Landsburg Diversion Dam when flows are less than 850 cfs.

(b) The measuring point for downramping rates at the Landsburg Diversion Dam will be the existing USGS Gage number 12117600 located below the Dam at river mile 20.4. Not later than the end of HCP Year 2, the City will install equipment to monitor this gage on a “real time” basis. For compliance purposes, specific ramping rate values set forth in this sub-section C.2.c. will be calculated from provisional real time data and gage error, as determined by USGS, shall be factored into the ramping rate calculation.

(c) The downramping rates and prescriptions set forth in this sub-section C.2.c. will not apply when flows exceed 850 cfs.

(2) Downramping During Normal Operations

(a) Between February 1 and October 31, the maximum downramping flow rate will be one inch per hour.

(b) Between November 1 and January 31, the maximum downramping flow rate will be two inches per hour.

(c) The tainter gates will be down and closed during normal operations.

(3) Downramping During Startup Following Full System Shutdown

(a) Based on past experience, full system shutdown at flows less than 850 cfs can be expected to occur one to two times per year for scheduled and unscheduled maintenance, and at least once per year for forebay cleaning. Shutdowns for construction may also occur depending on the nature of the construction project.

(b) To minimize risk of cavitation and mechanical damage of equipment at Landsburg Diversion Dam, initial downramping following full system shutdown will be at a maximum of 60 cfs per hour."

5.1.2 Compliance

During the 2024 reporting period, there were two formal downramping exceedance violations at USGS Gage 12117600 Cedar River below Landsburg. The exceedances occurred on October 17th between 4:30 am and 5:30 am and October 21st between 7:30 pm and 8:30 pm. The one-inch per hour downramping rate was exceeded by 0.32 inches and 2.12 inches, respectively. For the first downramping rate exceedance the Landsburg Forebay had a relatively high elevation and the operator switched the operating mode from automated to manual for a short period of time. This released some excess water before the flows returned to normal. In the second incident there was a natural increase in flows above Landsburg and a subsequent rise in the forebay level. The operational mode at the dam was switched from flow to level while the elevation of the forebay was excessively high. This caused a large quantity of water to be released, followed by sudden drop in flow.

All other downramping exceedances occurred when flows at the 12117600 Gage were above 850 cfs or during annual forebay cleaning operations and, therefore, did not result in a violation. See Table 8.1 and Figures 8.2 and 8.3.

Table 5.1.1 Downramping below Landsburg Dam: events that exceeded the maximum downramping flow rate of one inch per hour and less than 850 cfs between February 1 and October 31, 2003-2024.

Year/Date	Hour	Rate per Hour (inches)	Flow (cfs)	Comments/Explanations
2003				
2-May	8 pm	-1.2	278	Tainter gate operation error preparing for Landsburg Forebay cleaning
22-Oct	12 am	-1.08	802	Tainter gate operation error
28-Oct	8 pm	-1.2	354	Tainter gate operation error
31-Oct	11 am	-1.32	358	Downstream passage gate flow mode malfunction
2004				
11-Feb	8 pm	-1.08	727	Downstream passage gate opened too fast
26-May	6pm	-1.56	786	Operator Error
28-May	5pm	-1.08	443	Lake Youngs supply line 5 opened too fast
2005				
27-Mar	2 am	-1.08	332	Operator error trying to maximize diversion during large rain event
31-Oct	4pm	-1.2	535	Downstream passage gate opened too fast
2006				
Mar-21	5 pm	-1.32	374	Downstream passage gate opened too fast
2007				
1-Mar	7 am	-1.32	727	Operator error during closing of tainter gate
3-Oct	12 am	-1.08	625	Downstream passage gate opened too fast
3-Oct	1am	-1.56	563	Downstream passage gate opened too fast
2008				In Compliance with all rates
2009				
18-Aug	9 am	-1.2	136	Downstream Passage gate raised too fast
26-Oct	6 pm	-1.32	802	Decrease in generation flow during acute natural flow drop
28-Oct	8 pm	-1.44	325	Adjustment to set point for level mode on the downstream passage gate caused gate to rise too fast
2010				
18-Jun	11:30 pm	-1.08	611	Final adjustment on radial gate caused exceedance
4-Aug	9 pm	-1.2	217	Reopening of diversion after turbidity event combined with natural rapid decline in flows
2011				
5-Aug	7 pm	-1.08	108	Operator error switching from direct bypass mode to standard operating configuration
16-Sep	12:30 am	-1.92	165	Downstream Passage gate raised too fast
23-Oct	5 pm	-1.08	675	rapid change in diversion rate caused rise in forebay triggering excessive downstream passage gate adjustment
2012				In Compliance with all rates
2013				
24-Jul	2 pm	-2.64	140	Operator error during Downstream Passage Gate operation
16-Oct	10:15 pm	-1.2	480	Unanticipated fluctuations in automatic mechanism on Downstream Passage Gate
17-Oct	5pm	-1.56	416	Unanticipated fluctuations in automatic mechanism on Downstream Passage Gate
17-Oct	11:15 am	-1.32	381	Unanticipated fluctuations in automatic mechanism on Downstream Passage Gate
17-Oct	12:45 pm	-1.44	373	Unanticipated fluctuations in automatic mechanism on Downstream Passage Gate
2014				
7-Apr	2:15 pm	-1.68	815	Operator error
7-Apr	2:30 pm	-1.68	815	Operator error
3-Sep	1 pm	-1.56	429	Operator error
3-Sep	1:15 pm	-1.56	429	Operator error
3-Sep	2:30 pm	-1.08	394	Operator error
2015				In Compliance with all rates
2016				
24-Jun	10:30 am	-1.2	809	Operator error during Downstream Passage Gate operation
24-Jun	10:45 am	-1.2	755	Operator error during Downstream Passage Gate operation
2017				
1-Oct	4 am	-1.12	278	Operator error during Downstream Passage Gate operation
2018				In Compliance with all rates
2019				In Compliance with all rates
2020				
2-Jun	8 pm	-1.08	321	Operator error during forebay refill after forebay cleaning
2022				In Compliance with all rates
2023				
3-Mar	9 pm	-1.68	565	Operator error during Downstream Passage Gate operation
30-Mar	1 pm	-1.2	353	Operator error during Downstream Passage Gate operation
23-Apr	12 pm	-1.32	329	Operator error during Downstream Passage Gate operation
6-Jun	10 pm	-1.08	267	Operator error during Downstream Passage Gate operation
16-Jun	2 am	-1.44	314	Operator error during closing off diversion
16-Oct	7 pm	-1.2	254	Operator error during Downstream Passage Gate operation
2024				
17-Oct	4:30 am	-1.1	310	Operator error during a change from manual gate operation to automated gate operation
21-Oct	7:30 pm	-0.26	349	Operator error while switching Downstream Passage Gate from from flow to level operating mode

Table 5.1.2 Downramping below Landsburg Dam: Events exceeding the maximum downramping flow rate of two inches per hour and less than 850 cfs between November 1 and January 31, 2003-2024.

Year/Date	Hour	Rate per Hour (inches)	Flow (cfs)	Comments/Explanations
2003				
17-Nov	1 pm	-2.28	321	Operator error during Downstream Passage gate operation
2004				In Compliance
2005				In Compliance
2006				
12-Dec	2 pm	-2.28	786	Sluice gate at downstream end of V-screen opened too fast
2007				In Compliance
2008				In Compliance
2009				In Compliance
2010				In Compliance
2011				In Compliance
2012				In Compliance
2013				In Compliance
2014				In Compliance
2015				In Compliance
2016				In Compliance
2017				In Compliance
2018				In Compliance
2019				In Compliance
2020				In Compliance
2021				In Compliance
2022				
24-Dec	4 am	-2.16	407	Operator error while bringing down the forebay level and switching control to Automatic Level mode.
2023				In Compliance
2024				In Compliance

5.2 Downramping below Cedar Falls Powerhouse

5.2.1 Requirements

Required Downramping rates below Cedar Falls Powerhouse are specified in Section C.2.b in the IFA:

“(1) The measuring point for downramping rates at the Cedar Falls Powerhouse will be the existing USGS Gage number 12116500 located ½ mile below the Powerhouse at river mile 33.2. For compliance purposes, specific ramping rate values set forth in this sub-section C.2.b will be calculated from provisional real time data and gage error, as determined by USGS, and shall be factored into the ramping rate calculation.

(2) The downramping rates and prescriptions set forth in this sub-section C.2.b will not apply when flows exceed 300 cfs

b. Downramping During Normal Operations

(1) Between February 1 and June 15, the maximum downramping flow rate will be two inches per hour with no daylight downramping (defined as one hour before sunrise until one hour after sunset).

(2) Between June 16 and October 31, the maximum downramping flow rate will be one inch per hour.

(3) Between November 1 and January 31, the maximum downramping flow rate will be two inches per hour.

c. Downramping during full system shutdown

(1) Based on past experience, full system shutdown at flows less than 300 cfs can be expected to occur one to two times per year due to low flow conditions or for scheduled and unscheduled maintenance or construction projects.

(2) When the lone unit is shutdown the wicket gates close at a prescribed speed (a condition of the machine safety mechanisms), which results in a sudden drop in flow, averaging a total of 25 cfs per occurrence.

d. Swapping load during daytime downramping restrictions

(1) During daytime downramping restrictions there may be a need to swap loads between generators. In most circumstances it is seamless and would not show up as a change in stage. However, there are situations in moving water from one machine to the other, due to the normal shutdown sequence, that can cause a sudden drop followed by an increase, or vice-versa. These are typically short duration occurrences.

e. Extended shutdowns during the February to June 15 time frame.

(1) The City will notify the Commission ahead of time of circumstances that could require an extended shutdown of both generators and discuss the need for leniency on daytime downramping."

5.2.2 Compliance

During the 2024 reporting period, there was one downramping event on June 10, 2024.

Downramping was recorded during daylight hours during the daytime downramping restriction period. The event was initiated at the dam and was not caused by powerhouse operations. The downramp was recorded at USGS gage 12116500 one hour after the incident between 21:00 and 22:00 and was observed to be approximately 0.5 inch per hour. Restrictions on daytime downramping are designed to prevent stranding of juvenile Chinook. The change in flow was not recorded downstream at USGS gage 12117500 until June 11 at 00:15, which means the early downramp did not impact the Chinook redd locations during daytime hours. The cause of this event was human error.

As in years past, there were some minor, short-term fluctuations in flow and water surface elevation detected at USGS gage 12116500. Some of these events have been observed during the daytime downramping restriction period (February 1 through June 15). These events are infrequent, last for an hour or less and typically do not exceed 0.5 inch per hour. A detailed analysis determined that these fluctuations cannot be eliminated with the current turbines in place at the Cedar Falls Powerhouse. The turbines are set to operate within a range of 0.4 MWs. When the turbine drifts too far, a speeder motor nudges it back within range, but this operation is not highly accurate. These changes in flow are not caused by operations to ramp

generators or swap flows between generators. Upgrades to equipment, such as new digital generators, would be needed to improve the precision. Going forward, these small and brief fluctuations that are not associated with changes to operations will not be reported.

Table 5.2.1 Downramping below Cedar Falls Powerhouse: events exceeding no daytime downramping, and night time maximum downramping flow rate of two inches per hour and less than 300 cfs from February 1 to June 15, 2003-2024.

Year/Date	Time	Rate per hour (inches)	Flow (cfs)	Comments/Description
2003				In Compliance
2004				
16-Apr	6:30 am	-2.5	165	Emergency bypass system activated but provided insufficient flow
14-Jun	8:30 am	-1.9	122	Frequency excursion caused flow fluctuation
2005				
Apr-21	5:45 am	-2.2	32	Operator closed unit 5 and started up unit 6 causing drop in flow
2006	4:30 am	-0.4	53	Valve closure at Masonry Dam registered downstream during daylight hours
2007				In Compliance
2008				In Compliance
2009				In Compliance
2010				In Compliance
2011				In Compliance
2012				In Compliance
2013				In Compliance
2014				In Compliance
2015				
13-Jun	1 am	-4.2	150	During generator shutdown the unit would not trip off line
2016				In Compliance
2017				In Compliance
2018				In Compliance
2019				In Compliance
2020				In Compliance
2021				
29-Mar	1:45 pm to 3:30 pm	-2.0		Downramping occurred during daylight hours for 1.75 hours
2022				
14-Apr	8:45 PM	-2.8	177	Operator restarting generator, failed to match outflows when bringing the unit back online
15-Jul				
2023				In Compliance
2024				
June 10	9:00 PM	Daytime Downramp		Operator initiated downramping 2 hours early during period of daytime downramping restrictions

Table 5.2.2 Downramping below Cedar Falls Powerhouse: events exceeding maximum downramping flow rate of one inch per hour and less than 300 cfs between June 16 and October 31, 2003-2024.

Year/Date	Time	Rate per hour (inches)	Flow (cfs)	Comments/Description
2003				
Oct-21	9 am	-1.4	116	Operator Error
2004				In Compliance
2005				In Compliance
2006				In Compliance
2007				In Compliance
2008				In Compliance
2009				In Compliance
2010				In Compliance
2011				In Compliance
2012				In Compliance
2013				In Compliance
2014				In Compliance
2015				
Jul-21	11:30 am	-1.1	74	Unit downramped to speed-no-load (less than 25 cfs) during low flow period
2016				In Compliance
2017				
Jul-19	10:30 am	-1.1	107	Unplanned valve position change of 48" Masonry Spill Valve
Sep-21	1:15 pm	-1.2	95	SOPs ignored: Gen 5 brought online while 48" spill valve at dam was closing
Oct-20	6:45 am	-1.1	156	Occurred during last hour of 15 hour downramp during flow recession after heavy rain
2018				
Jul-26	9:45 am	-1.2	67	SOP for downramping when unit generating less than 1MW were not followed
2019				In Compliance
2020				In Compliance
2021				In Compliance
2022				In Compliance
2023				In Compliance
2024				In Compliance

Table 5.2.3 Downramping below Cedar Falls Powerhouse: events exceeding maximum downramping flow rate of one inch per hour and less than 300 cfs June 16th and January 31 and November 1 through December 31, 2003-2024.

Year/Date	Time	Rate per hour (inches)	Flow (cfs)	Comments/Description
2003				In Compliance
2004				In Compliance
2005				In Compliance
2006				In Compliance
2007				In Compliance
2008				In Compliance
2009				
Apr-30	2:15 am	-1.7	79	Operator failed SOP to reduce downramping rate when flows reached 90 cfs
2010				In Compliance
2011				In Compliance
2012				In Compliance
2013				In Compliance
2014				In Compliance
2015				In Compliance
2016				In Compliance
2017				
Jul-19	10:30 -10:45 am	-1.3-1.9	74-78	Unplanned valve position change of 48" Masonry Spill Valve
2018				In Compliance
2019				In Compliance
2020				In Compliance
2021				In Compliance
2022				In Compliance
2023				In Compliance
2024				In Compliance

5.3 Downramping below Masonry Dam

5.3.1 Requirements

Required Downramping rates below Masonry Dam are specified in Section C.2.a in IFA:

“(1) The measuring point for downramping rates at the Masonry Dam will be the USGS Gage number 12116400 located below the Dam at river mile 33.7. For compliance purposes, specific ramping rate values set forth in this sub-section C.2.a will be calculated from provisional real time data and gage error, as determined by USGS, and shall be factored into the ramping rate calculation.

(2) The downramping rates and prescriptions set forth in this sub-section C.2.a will not apply when flows exceed 80 cfs

b. Downramping During Normal Operations

(1) Between February 1 and October 31 the final maximum downramping flow rate will be one-inch per hour.

(2) Between November 1 and January 31, the maximum downramping flow rate will be two inches per hour.”

5.3.2 Compliance

During the 2024 reporting period, downramping below the Masonry Dam was in compliance with the IFA at USGS Gage 12116400. See Figures 8.6 and 8.7.

For long term tracking of the City’s performance in meeting downramping requirements below Masonry Dam see Table 5.3.1.

Table 5.3.1 Downramping compliance below Masonry Dam, 2003 – 2024.

Year/Date	Time	Rate per hour (inches)	Flow (cfs)	Comments/Description
2003				In Compliance
2004				In Compliance
2005				In Compliance
2006				In Compliance
2007				In Compliance
2008				In Compliance
2009				In Compliance
Apr-30	2:15 am	-1.7	79	Operator failed SOP to reduce downramping rate when flows reached 90 cfs
2010				In Compliance
2011				In Compliance
2012				In Compliance
2013				In Compliance
2014				In Compliance
2015				In Compliance
2016				In Compliance
2017				In Compliance
Jul-19	10:30 -10:45 am	-1.3-1.9	74-78	Unplanned valve position change of 48" Masonry Spill Valve
2018				In Compliance
2019				In Compliance
2020				In Compliance
2021				In Compliance
2022				In Compliance
2023				In Compliance
2024				In Compliance

6. Emergency Bypass Capability

6.1 Emergency Bypass Requirements

Emergency bypass Capabilities are specified in Section C.2.a in IFA:

In 1999, the City installed, tested and implemented operating procedures for new equipment to provide bypass flows around its hydroelectric turbines during most emergency plant shutdowns to protect against stranding of fish and dewatering of redds as a result of such events.

In its original configuration, the Cedar Falls Hydroelectric Project was not able to provide flow to the river during emergency shutdown of electrical generating equipment. To remedy this situation, in early 1999, the City installed equipment to provide bypass flows around its hydroelectric turbines during most emergency plant shutdowns. This original bypass system's flow capacity was limited to approximately 70% of the original flow passing through the generator prior to the load rejection. The City decided to expand the emergency bypass system's scope to improve the flow capacity through the bypass system. This work was completed in 2002 and has resulted in a more reliable system that has provided matching flow continuation to the river during most emergency shutdowns.

6.2 Compliance

During the 2024 reporting period there were no emergency shutdowns at the powerhouse. The Cedar Falls Powerhouse was not in operation until the last two weeks of December, 2024, while the new substation was being completed. When the generators returned to operation on December 16, 2024, the equipment to provide bypass flows was tested and found to be working properly.

For long term tracking of the City's performance using the Emergency Bypass Capability, see Table 6.2.1.

Table 6.2.1 Emergency Bypass Activations 2003-2024

Year	# of Emergency Bypass Activations	# of Activations with Complete Flow Continuation	# of Unsuccessful Activations/EB failure	Comments/Descriptions (DRE = Downramping Exceedance)
2003	0	0	0	
2004	1	0	1	flow continuation did not match pre-event flows resulting in DRE
2005	0	0	0	Loss of generator and transmission line power during a windstorm prevented activation, DRE
2006	0	0	0	
2007	1	0	1	Emergency bypass equipment did not function properly during emergency plant shutdown, DRE
2008	4	1	3	on 2 occasions only partial flow continuation and on one occasion EB failed, DRE
2009	4	4	0	
2010	10	9	1	Both units tripped offline and one unit's relief valve lost air, gripper shut the valve, DRE
2011	2	2	0	
2012	3	3	0	
2013	9	9	0	
2014	2	2	0	
2015	2	1	1	Sudden load reduction to one unit caused relief valve to close resulting in DRE
2016	5	5	0	
2017	13	12	1	Activated EB but butterfly valve began to close, operator intervened manually no DRE
2018	5	5	0	
2019	0	0	0	
2020	0	0	0	
2021	6	6	0	
2022	8	8	0	
2023	0	0	0	

7. Municipal Water Use

7.1 Requirements

In 2020, the City's maximum diversion rate from the Cedar River, as described in the Muckleshoot Settlement, changed from 105 MGD to 110 MGD. The new maximum rate is in effect until 2030.

7.2 Compliance

The City was in compliance with the provision in 2024. Actual average annual water diversion in 2023 was 90.7 MGD. The City was relying on Cedar River water more than usual for water supply due to the South Fork Tolt Reservoir being well below normal elevations for most of 2023. See Table 8.7. For long term tracking of the City's annual average water diversion at Landsburg Dam on the Cedar River, see Table 7.2.1.

Table 7.2.1 Municipal Water Use: annual average water Diversion at Landsburg Dam on the Cedar River, 2001-2024.

Year	Annual Average Daily Water Diversion (MGD)	Year	Annual Average Daily Water Diversion (MGD)
2001	89.6	2013	72.8
2002	78.6	2014	72.7
2003	81.7	2015	77.6
2004	85.9	2016	79.7
2005	78.7	2017	78.7
2006	81.9	2018	78.3
2007	79.3	2019	84.6
2008	77.4	2020	74.5
2009	81.4	2021	76.8
2010	75	2022	73.3
2011	72.1	2023	90.7
2012	73.7	2024	79.6

7.3 Municipal Water Service Area

The retail service and wholesale service areas remained the same as in 2022.

8. Measurement and Reporting

Annual reports are provided to the Commission to evaluate the City's compliance with the terms of the Instream Flow Agreement Section D.3.a:

“The City will provide to the Commission, on an annual basis, the record of measurements from the locations listed in subsection D.1. Average daily flows and reservoir elevations will be provided to indicate compliance with minimum instream flow requirements and goals. A table will be provided to show flows at the measuring points compared to the critical, low-normal, high-normal, and non-firm flow levels as identified in section B. For periods affected by downramping operations, flow data will be provided in one-hour increments to indicate compliance with downramping prescriptions.”

These flow and elevation records are described in the following compliance graphs and tables:

Figure 8.1 – Instream Flows Below Landsburg
Figure 8.2 – Downramping Flows Below Landsburg
Figure 8.3 – Downramping Rate of Change Below Landsburg
Figure 8.4 – Downramping Flows below Powerhouse
Figure 8.5 – Downramping Rate of Change Below Powerhouse
Figure 8.6 – Downramping Flows below Masonry Dam
Figure 8.7 – Downramping Rate of Change Below Masonry Dam

Table 8.1 – USGS 12117600 Mean Daily Flows
Table 8.2 – Instream Schedule with Firm and Non-Firm Flows
Table 8.3 – USGS 12116500 Mean Daily Flows
Table 8.4 – USGS 12116400 Mean Daily Flows
Table 8.5 – SPU Chester Morse Reservoir Daily 7AM Elevation
Table 8.6 – USGS 12115000 Mean Daily Flows
Table 8.7 – SPU Landsburg Daily Diversion
Table 8.8 – SPU Landsburg 24 Hour Total Precipitation
Table 8.9 – SPU Masonry Dam 24 Hour Precipitation

Figure 8.1 – Instream Flows Below Landsburg Compliance USGS Gage 12117600

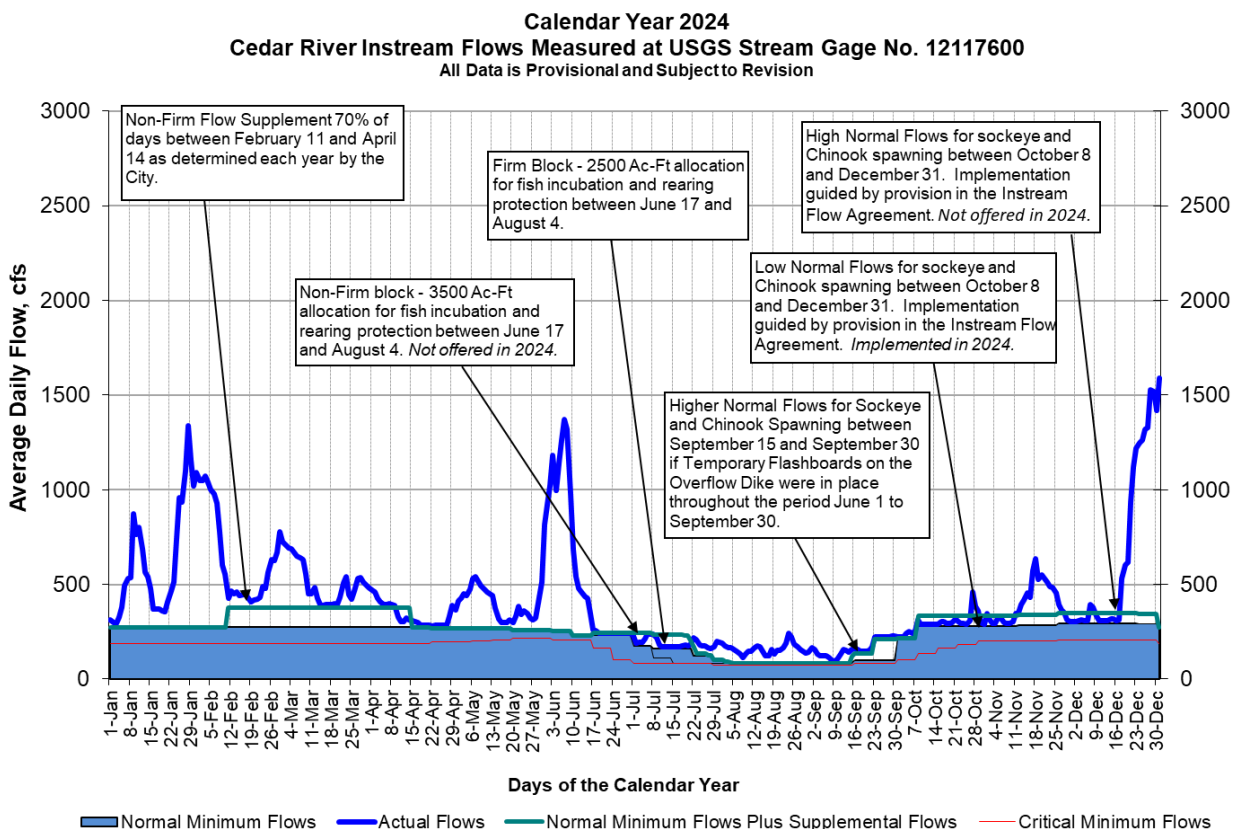


Figure 8.2 – Downramping Flows Below Landsburg Compliance Graph

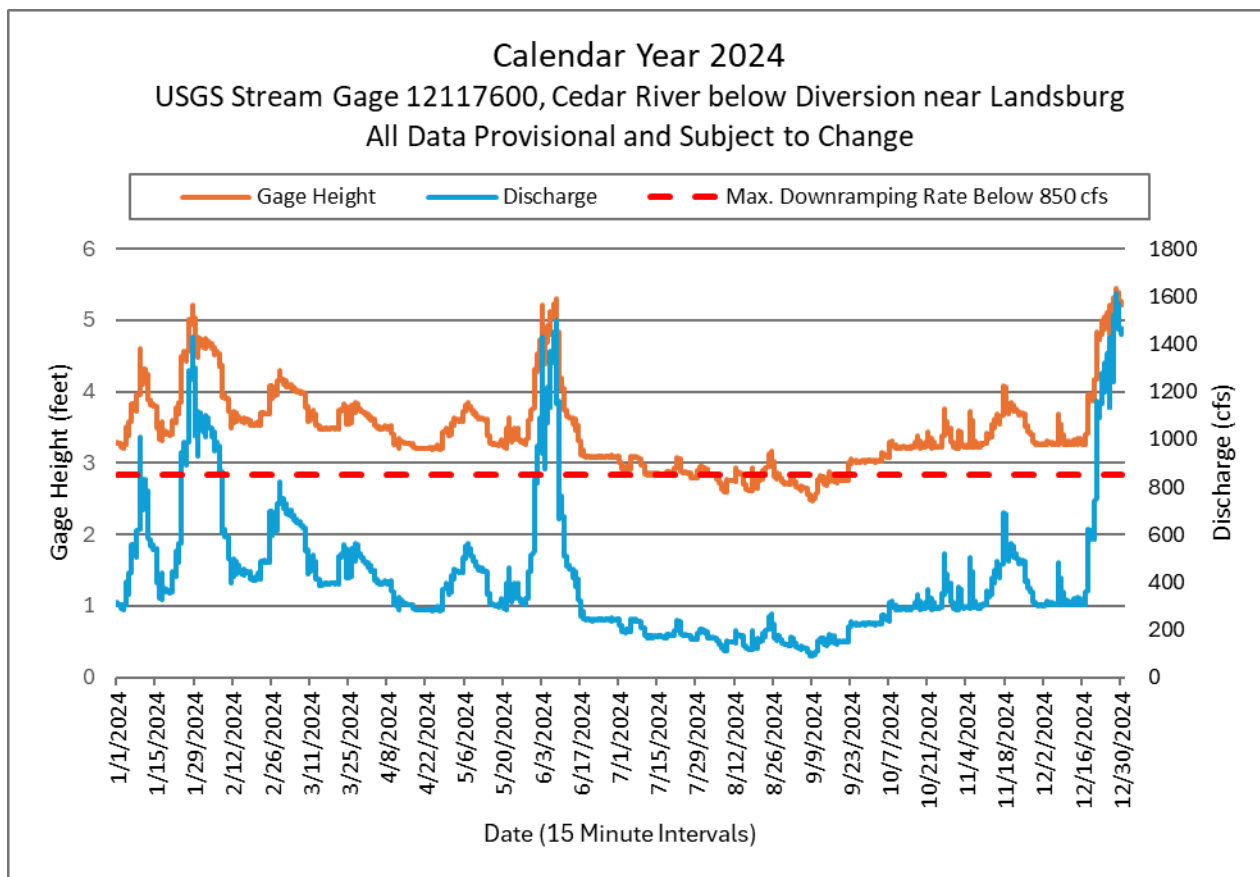


Figure 8.3 – Downramping Rate of Change Below Landsburg Compliance Graph

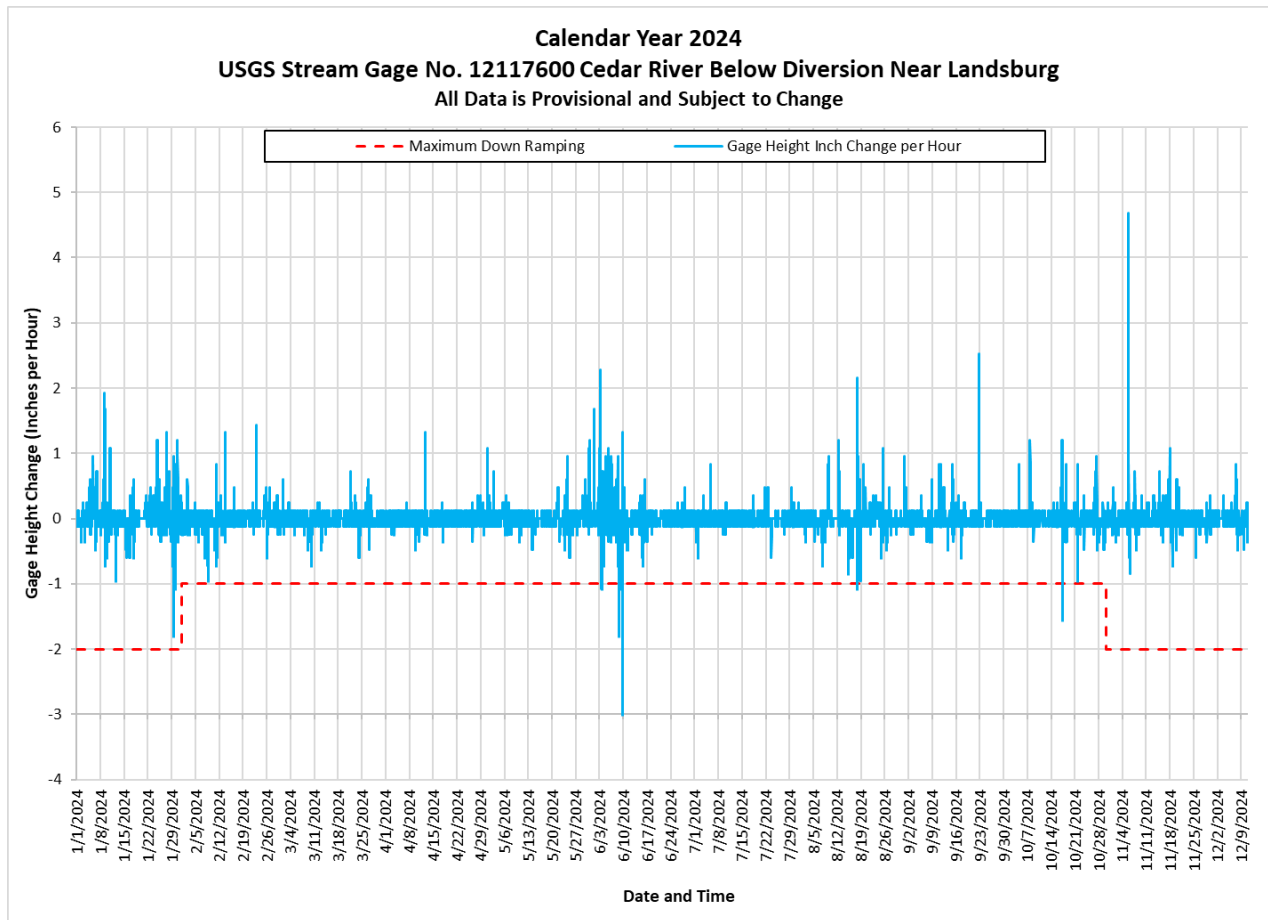
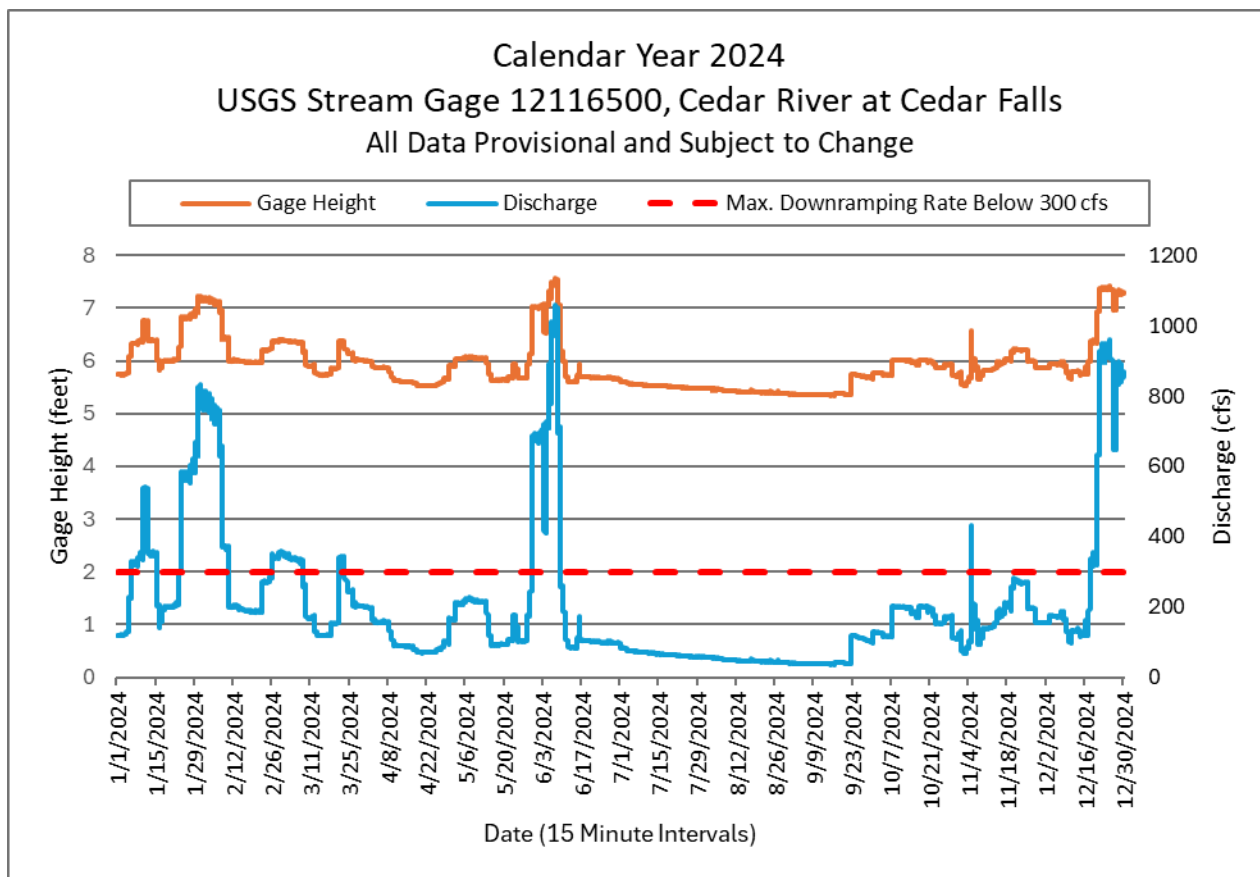


Figure 8.4 – Downramping Flows below Powerhouse Compliance Graph



**Figure 8.5 – Downramping Rate of Change Below Powerhouse Compliance
Graph**

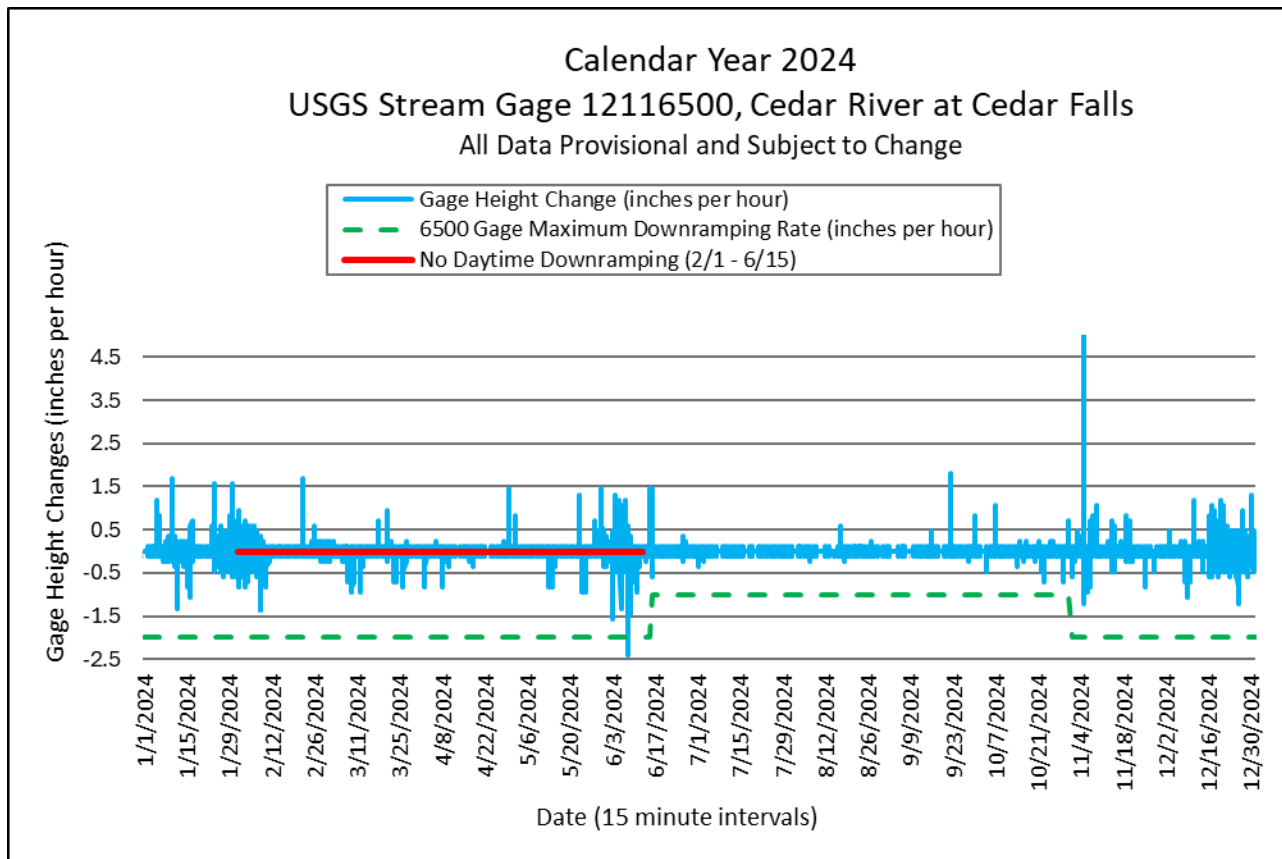


Figure 8.6 – Downramping Flows below Masonry Dam Compliance Graph

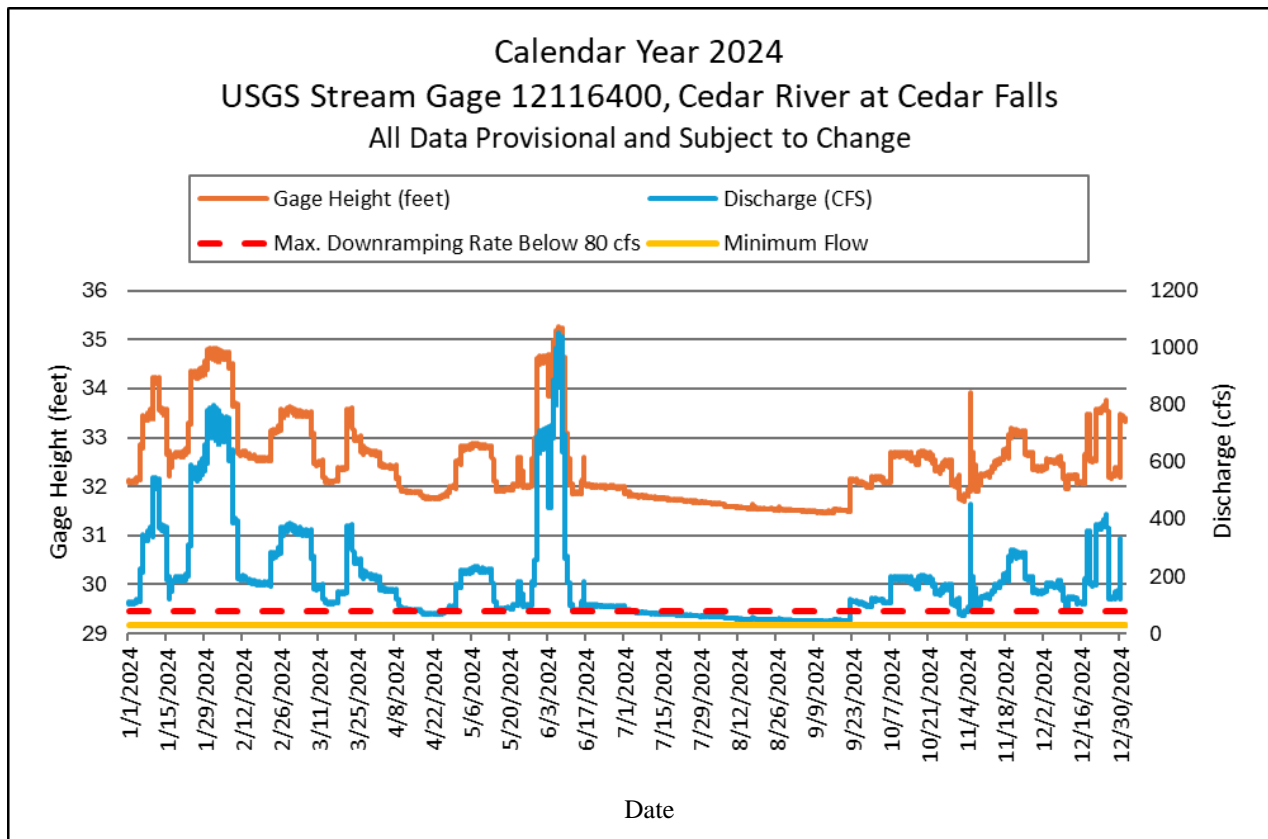


Figure 8.7 – Downramping Rate of Change Below Masonry Dam Compliance Graph

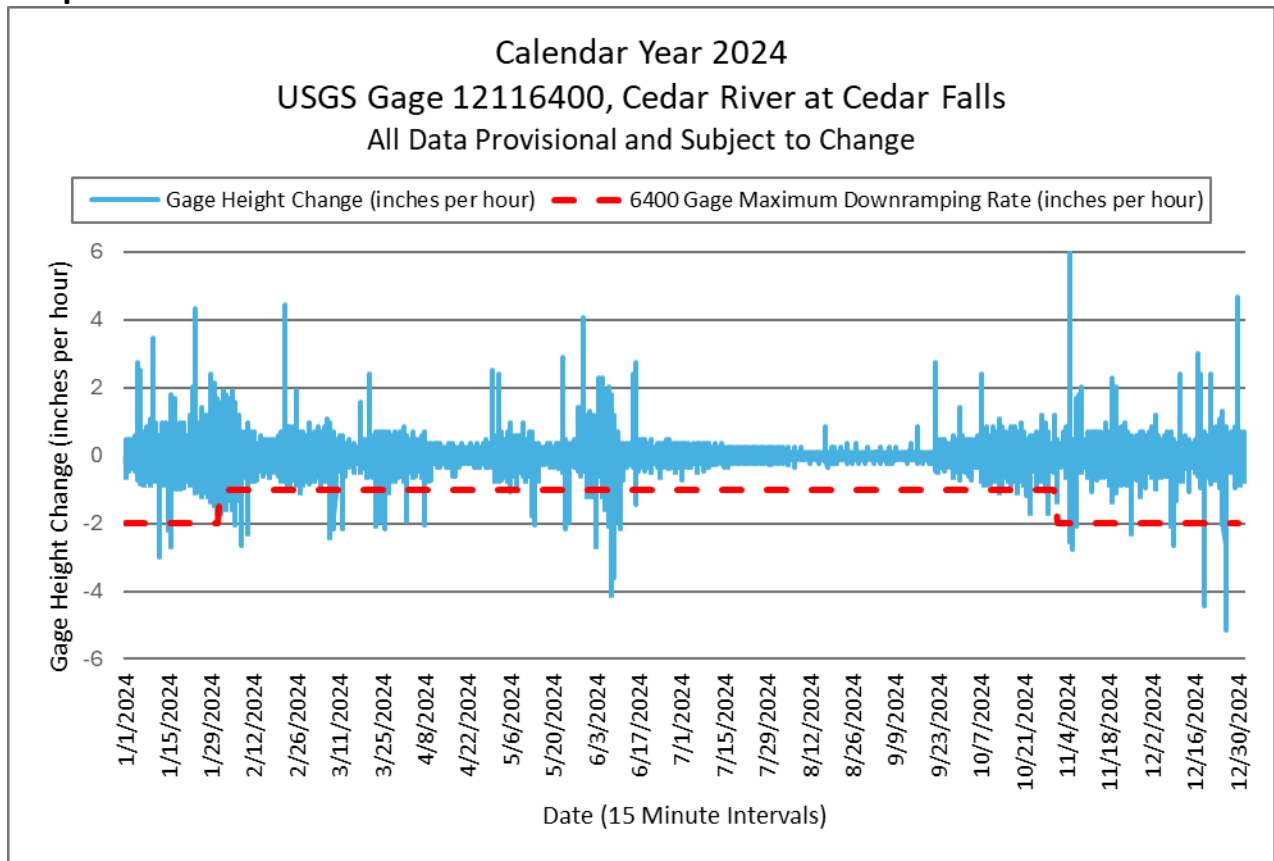


Table 8.1												
U.S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY - WATER RESOURCES												
STATION NUMBER 12117600 CEDAR RIVER BELOW DIVERSION NEAR LANDSBURG, WA												
SOURCE AGENCY USGS STATE 53 COUNTY 033												
LATITUDE 472247 LONGITUDE 1215856 NAD27 DRAINAGE AREA 124 sq. mi. DATUM 490 NGVD29												
Daily Discharge, cubic feet per second												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
DAILY MEAN VALUES												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	311	1050	728	472	414	920	226	188	164	225	345	303
2	299	1050	707	459	429	1020	191	177	155	225	314	303
3	293	1070	691	428	449	1180	193	166	133	225	294	308
4	329	1040	688	406	443	998	196	166	123	244	294	313
5	380	1000	667	396	474	1140	212	158	122	250	334	308
6	495	976	652	393	530	1260	241	145	123	244	317	306
7	532	932	642	399	543	1370	239	131	113	258	301	395
8	534	780	633	395	517	1320	236	114	97.2	311	292	379
9	873	602	556	389	495	979	217	135	96.2	291	296	334
10	765	553	453	326	473	682	178	149	102	288	304	310
11	800	425	449	304	458	540	172	147	134	288	345	309
12	690	465	484	305	453	480	173	166	157	289	351	309
13	564	453	425	322	448	459	171	174	151	288	392	307
14	543	460	396	315	374	438	173	172	143	288	417	316
15	480	443	391	308	322	425	173	149	158	290	457	318
16	370	445	393	305	306	348	171	125	159	302	430	308
17	370	445	394	299	301	262	169	123	157	302	575	313
18	368	429	395	285	302	257	177	156	147	296	635	529
19	360	410	397	283	319	243	178	131	149	292	526	603
20	357	416	394	283	297	243	176	154	149	297	550	618
21	408	421	432	283	334	243	183	152	151	316	529	933
22	467	433	507	282	385	242	217	164	169	304	512	1120
23	514	487	542	283	340	243	208	192	222	294	490	1220
24	741	481	446	283	362	243	180	242	221	292	483	1250
25	957	566	424	284	345	243	176	222	222	291	454	1260
26	934	630	463	286	323	244	175	187	223	309	393	1320
27	1100	624	529	284	314	243	166	169	225	462	365	1330
28	1340	668	534	334	321	243	159	158	225	384	349	1530
29	1160	776	513	387	401	242	173	147	226	362	311	1520
30	1020		497	364	514	244	197	139	226	298	303	1420
31	1090	---	483		818	---	193	140	---	287	---	1590
TOTAL	19444	18530	15905	10142	12804	16994	5889	4938	4842	9092	11958	21682
MEAN	627	639	513	338	413	566	190	159	161	293	399	699
MAX	1340	1070	728	472	818	1370	241	242	226	462	635	1590
MIN	293	410	391	282	297	242	159	114	96	225	292	303

Table 8.2												
SEATTLE PUBLIC UTILITIES												
OPERATIONAL MINIMUM INSTREAM FLOW SCHEDULE WITH FIRM AND NON-FIRM FLOWS												
STATION NUMBER 12117600 CEDAR RIVER BELOW DIVERSION NEAR LANDSBURG, WA												
SOURCE AGENCY SPU - (With Walsh Ditch adjustment)												
LATITUDE 472247 LONGITUDE 1215856 NAD27 DRAINAGE AREA 124 sq. mi. DATUM 490 NGVD29												
All Data is Provisional and Subject to Revision												
Discharge, cubic feet per second												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
DAILY MEAN VALUES												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	275	275	378	378	268	258	244	85	83	214	334	347
2	275	275	378	378	268	258	244	85	83	214	334	347
3	275	275	378	378	268	256	244	83	83	214	334	347
4	275	275	378	378	268	256	244	83	83	214	334	347
5	275	275	378	378	268	256	244	83	83	214	334	347
6	275	275	378	378	268	256	244	83	83	214	334	347
7	275	275	378	378	268	256	244	83	83	214	334	347
8	275	275	378	378	268	256	244	83	83	334	334	347
9	275	275	378	378	268	256	244	83	83	334	334	347
10	275	275	378	378	268	231	244	83	83	334	334	347
11	275	378	378	378	268	231	244	83	83	334	334	347
12	275	378	378	378	268	231	244	83	83	334	339	347
13	275	378	378	378	268	231	244	83	83	334	339	347
14	275	378	378	378	268	231	244	83	83	334	339	347
15	275	378	378	273	268	231	244	83	121	334	339	347
16	275	378	378	273	268	231	244	83	136	334	339	347
17	275	378	378	273	268	244	244	83	136	334	339	347
18	275	378	378	273	268	244	244	83	136	334	339	347
19	275	378	378	273	268	244	212	83	136	334	339	347
20	275	378	378	273	258	244	212	83	136	334	339	347
21	275	378	378	273	258	244	180	83	136	334	339	347
22	275	378	378	268	258	244	180	83	136	334	339	347
23	275	378	378	268	258	244	148	83	213	334	339	347
24	275	378	378	268	258	244	148	83	213	334	339	345
25	275	378	378	268	258	244	124	83	213	334	339	345
26	275	378	378	268	258	244	124	83	213	334	347	345
27	275	378	378	268	258	244	116	83	213	334	347	345
28	275	378	378	268	258	244	108	83	213	334	347	345
29	275	---	378	268	258	244	108	83	213	334	347	345
30	275	---	378	268	258	244	108	83	213	334	347	345
31	275	---	378	---	258	---	85	83	---	334	---	275
TOTAL	8525	9554	11718	9615	8188	7341	6245	2577	3939	9514	10155	10671
MEAN	275	339	378	322	264	245	202	83	128	306	338	344
MAX	275	378	378	378	268	258	244	85	213	334	347	347
MIN	275	275	378	268	258	231	85	83	83	214	334	275
AC-FT	16557	18555	22758	18674	15902	14257	12129	5005	7650	18478	19723	20725

Table 8.3												
U.S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY - WATER RESOURCES												
STATION NUMBER 12116500 CEDAR RIVER AT CEDAR FALLS, WA												
SOURCE AGENCY USGS STATE 53 COUNTY 033												
LATITUDE 472502 LONGITUDE 1214727 NAD27 DRAINAGE AREA 84.2 sq. mi. DATUM 902.10 NGVD29												
Discharge, cubic feet per second												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
DAILY MEAN VALUES												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	158	785	351	197	166	682	90	56	41	128	118	154
2	120	779	345	193	186	689	82	56	40	126	71	154
3	120	770	341	159	210	552	80	56	40	126	75	166
4	125	758	339	158	209	536	76	55	40	120	93	175
5	169	745	336	157	211	803	74	55	40	116	201	174
6	259	742	334	157	218	930	74	55	39	116	143	172
7	322	699	332	158	223	1019	73	53	38	151	129	181
8	323	514	323	156	219	863	72	49	38	199	104	175
9	344	369	252	116	216	482	71	48	38	199	127	146
10	406	313	167	93	214	251	70	48	38	198	137	114
11	527	198	168	91	213	117	70	48	38	198	140	119
12	418	204	170	89	213	87	69	47	37	198	142	133
13	352	201	122	88	212	84	68	46	37	198	151	133
14	351	196	119	88	129	83	68	46	38	190	166	125
15	265	192	118	88	94	84	67	46	37	184	175	118
16	173	190	118	87	91	157	66	46	39	180	176	134
17	180	188	120	86	92	105	66	46	43	177	197	131
18	197	188	134	72	92	104	65	46	42	201	205	289
19	199	187	152	71	94	103	64	45	41	200	216	335
20	198	188	152	71	92	103	64	45	41	195	272	403
21	203	187	254	71	98	102	63	44	40	191	274	779
22	209	219	340	71	106	100	62	43	85	183	271	923
23	225	271	338	71	134	101	62	44	119	164	268	921
24	446	271	247	71	175	99	62	45	116	152	268	930
25	570	281	245	75	107	98	60	43	114	153	229	932
26	569	312	245	78	103	98	60	43	111	159	196	689
27	576	341	206	82	103	99	59	44	109	172	195	733
28	601	347	206	95	122	98	58	43	106	171	180	861
29	622	357	203	102	187	97	59	42	102	145	156	868
30	710		200	113	338	97	59	41	114	111	156	946
31	791		198		685		58	41		116		1074
TOTAL	10728	10992	7175	3204	5553	8824	2087	1466	1803	5118	5233	13189
MEAN	346	379	231	107	179	294	67	47	60	165	174	425
MAX	791	785	351	197	685	1019	90	56	119	201	274	1074
MIN	120	187	118	71	91	83	58	41	37	111	71	114

Table 8.4												
U.S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY - WATER RESOURCES												
STATION NUMBER 12116400 CEDAR RIVER AT CEDAR FALLS, WA												
SOURCE AGENCY USGS STATE 53 COUNTY 033												
LATITUDE 472508 LONGITUDE 1214649 NAD27 DRAINAGE AREA 83.9 sq. mi. DATUM 940 NGVD29												
Discharge, cubic feet per second												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
DAILY MEAN VALUES												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	220	743	373	197	166	676	88	60	45	120	108	146
2	106	742	366	193	190	681	81	59	45	119	67	148
3	106	730	360	155	216	562	79	59	45	118	71	162
4	111	726	358	153	215	552	76	58	44	112	82	172
5	158	717	355	153	218	798	75	58	44	109	195	171
6	260	718	354	151	225	903	74	57	44	109	132	168
7	335	676	354	151	230	971	73	56	44	147	119	177
8	336	521	341	148	227	821	73	53	43	194	95	170
9	360	395	254	107	223	479	72	52	43	195	118	137
10	423	324	158	87	222	260	71	52	43	194	127	105
11	532	192	159	85	221	111	71	51	43	195	131	109
12	431	198	160	84	220	84	70	51	42	194	133	123
13	370	193	110	83	218	81	70	51	42	193	144	123
14	367	185	107	83	125	81	69	50	42	185	156	114
15	267	180	105	83	89	82	69	50	42	178	167	107
16	162	178	106	83	87	155	68	50	44	173	171	107
17	171	174	109	82	87	100	67	50	47	171	194	116
18	188	173	124	70	88	99	67	50	46	197	203	303
19	191	172	144	70	90	98	66	49	46	197	215	227
20	191	173	143	70	88	98	66	49	45	190	278	174
21	196	174	268	70	93	98	65	48	44	187	283	247
22	201	211	372	70	100	97	65	48	84	178	279	373
23	220	277	369	69	132	97	64	48	113	157	277	374
24	459	276	254	70	174	96	64	49	110	144	276	388
25	563	287	252	72	101	95	63	47	108	145	232	391
26	558	324	252	76	98	94	63	47	105	151	195	149
27	568	361	208	79	97	95	62	48	103	165	194	123
28	589	367	208	90	118	94	62	47	100	165	176	134
29	608	379	205	96	190	94	61	46	97	138	149	140
30	679		202	109	357	95	61	46	108	101	145	214
31	750		200		678		60	46		107		343
TOTAL	10680	10764	7331	3089	5584	8646	2136	1582	1853	4928	5112	5935
MEAN	345	371	236	103	180	288	69	51	62	159	170	191
MAX	750	743	373	197	678	971	88	60	113	197	283	391
MIN	106	172	105	69	87	81	60	46	42	101	67	105

Table 8.5												
SEATTLE PUBLIC UTILITIES												
CHESTER MORSE LAKE - DAILY 7AM ELEVATION												
SOURCE AGENCY USGS												
LATITUDE 472434 LONGITUDE 1214322 NAD27 DRAINAGE AREA 78.4 sq mi*												
Elevation, Feet												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
Daily Water Level												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	1551.8	1555.7	1555.2	1557.2	1561.7	1564.2	1563.18_E	1557.4	1552.3	1550.1	1547.4	1551.1
2	1551.8	1555.9	1555.4	1557.2	1561.8	1563.7	1563.19_E	1557.2	1552.3	1550.0	1547.8	1551.0
3	1551.8	1555.8	1555.5	1557.3	1561.8	1564.3	1563.19_E	1557.0	1552.3	1549.9	1548.2	1550.9
4	1551.9	1555.5	1555.5	1557.4	1561.8	1564.6	1563.18_E	1556.8	1551.8	1549.8	1548.7	1550.7
5	1552.1	1555.2	1555.4	1557.4	1561.8	1565.3	1563.18_E	1556.7	1551.7	1549.7	1549.1	1550.5
6	1552.3	1554.7	1555.2	1557.4	1562.0	1565.1	1563.18_E	1556.5	1551.5	1549.6	1549.6	1550.6
7	1552.3	1554.3	1555.0	1557.5	1562.3	1564.8	1563.18_E	1556.5	1551.3	1549.5	1549.8	1550.7
8	1552.2	1553.9	1554.8	1557.5	1562.6	1564.6	1563.18_E	1556.5	1551.2	1549.3	1549.9	1551.1
9	1552.5	1553.7	1554.6	1557.8	1562.8	1564.2	1563.18_E	1556.0	1551.0	1549.1	1550.0	1551.3
10	1552.8	1553.5	1554.5	1558.3	1562.9	1564.2	1561.8	1555.8	1550.9	1548.9	1550.1	1551.4
11	1552.7	1553.4	1554.5	1558.7	1563.0	1564.2	1561.6	1555.6	1550.7	1548.6	1550.3	1551.5
12	1552.6	1553.6	1554.5	1559.0	1563.2	1564.2	1561.4	1555.4	1550.6	1548.4	1550.4	1551.6
13	1552.6	1553.7	1554.7	1559.2	1563.3	1564.2	1561.2	1555.2	1550.5	1548.1	1550.7	1551.6
14	1552.2	1553.8	1554.8	1559.4	1563.4	1564.2	1561.0	1555.0	1550.4	1547.9	1551.0	1551.6
15	1552.0	1553.7	1554.8	1559.6	1563.5	1564.2	1560.8	1554.8	1550.4	1547.7	1551.2	1551.7
16	1551.9	1553.8	1554.8	1559.8	1563.6	1564.2	1560.6	1554.6	1550.4	1547.5	1551.2	1551.7
17	1551.9	1553.7	1554.9	1560.0	1563.7	1564.2	1560.4	1554.2	1550.4	1547.4	1551.4	1551.7
18	1552.0	1553.6	1555.1	1560.0	1563.8	1564.2	1560.2	1554.3	1550.3	1547.2	1551.9	1551.9
19	1551.8	1553.5	1555.3	1560.1	1563.8	1564.2	1560.0	1554.2	1550.3	1547.1	1552.3	1552.6
20	1551.7	1553.4	1555.6	1560.2	1563.8	1564.2	1559.8	1554.0	1550.3	1547.0	1552.3	1552.9
21	1551.6	1553.4	1555.9	1560.1	1563.8	1564.1	1559.5	1553.9	1550.3	1546.9	1552.2	1552.8
22	1551.6	1553.3	1555.9	1560.1	1564.1	1564.1	1559.3	1553.7	1550.2	1546.8	1552.1	1552.4
23	1551.6	1553.2	1556.0	1560.1	1564.4	1564.0	1559.1	1553.5	1550.2	1546.6	1552.0	1552.1
24	1551.8	1553.0	1556.0	1560.1	1564.4	1563.9	1558.9	1553.4	1550.2	1546.5	1551.9	1552.0
25	1551.9	1552.9	1556.2	1560.1	1564.5	1563.8	1558.7	1553.3	1550.2	1546.5	1551.7	1551.8
26	1551.9	1553.5	1556.3	1560.3	1564.6	1563.6	1558.5	1553.2	1550.3	1546.3	1551.6	1551.8
27	1552.0	1553.9	1556.5	1560.4	1564.7	1563.6	1558.3	1553.1	1550.3	1546.4	1551.5	1552.4
28	1552.8	1554.1	1556.9	1560.7	1564.8	1563.5	1558.1	1552.9	1550.3	1546.7	1551.4	1552.8
29	1554.2	1554.7	1557.1	1561.1	1564.8	1563.4	1557.9	1552.8	1550.2	1546.9	1551.3	1553.8
30	1555.0	---	1557.2	1561.5	1564.9	1563.2	1557.8	1552.6	1550.2	1547.1	1551.2	1554.3
31	1555.5	---	1557.2	---	1564.6	---	1557.6	1552.4	---	1547.2	---	1554.3
TOTAL	48122.5	45066.3	48221.0	46775.8	48466.1	46923.9	34312.0	48198.4	46522.9	47986.5	46520.2	48108.4
MEAN	1552	1554	1556	1559	1563	1564	1560	1555	1551	1548	1551	1552
MAX	1555	1556	1557	1561	1565	1565	1562	1557	1552	1550	1552	1554
MIN	1552	1553	1555	1557	1562	1563	1558	1552	1550	1546	1547	1551

Table 8.6+A1:M41A9A1:M48A1:												
U.S. DEPARTMENT OF THE INTERIOR - U.S. GEOLOGICAL SURVEY - WATER RESOURCES												
Retrieved from SPU IMS SCADA Database: 2022-03-03												
STATION NUMBER 12115000 CEDAR RIVER NEAR CEDAR FALLS,WA												
SOURCE AGENCY USGS STATE 53 COUNTY 033												
LATITUDE 472213 LONGITUDE 1213726 NAD27 DRAINAGE AREA 40.7 sq. mi. DATUM 1560.0 NGVD29												
All Data is Provisional and Subject to Revision												
Discharge, cubic feet per second												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
DAILY MEAN VALUES												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	170	748	474	229	323	269	126	48.3	33.4	25.5	109	119
2	166	625	380	223	302	331	120	46.1	33	25	165	111
3	166	499	313	264	282	757	114	44.8	32.5	24.9	171	105
4	184	413	271	255	281	827	108	43.6	32.1	25.9	215	98.9
5	205	355	234	240	301	814	102	42.4	31.3	27.3	229	94.3
6	222	314	208	223	353	602	97.7	41.4	30.5	28.3	175	90.7
7	204	277	189	227	376	487	93.5	41	30	26.8	143	174
8	195	250	179	229	353	426	90.1	40.1	29.8	25.8	124	264
9	312	233	171	434	335	374	87	39.3	29.3	25.1	115	234
10	279	212	169	433	376	330	84.5	38.4	28.7	24.6	110	204
11	239	209	175	381	473	288	81.6	37.9	30.3	24.3	128	183
12	204	240	200	345	493	257	78.8	38	32.2	23.5	168	166
13	170	227	194	328	421	231	75.3	37.7	31.5	22.9	272	153
14	165	214	180	347	370	211	72.4	37.5	31.7	22.7	313	142
15	160	202	173	355	380	225	68.6	37.4	33.2	23.2	290	138
16	153	188	183	319	388	230	64.6	37.3	32.1	25.1	247	130
17	150	177	222	276	344	224	63.3	37.4	30.6	30.6	486	142
18	146	169	290	244	289	239	61.2	45.8	29.6	35.1	479	405
19	139	162	374	221	259	219	58.9	40.4	28.5	44.2	348	368
20	129	162	415	206	233	207	56.9	38.6	27.8	51.5	275	310
21	132	161	388	199	264	197	56.6	38.6	27.6	57.6	227	295
22	145	154	355	187	379	184	56.1	37.6	27	49.3	243	320
23	165	147	355	179	320	173	54.3	39.9	26.4	42.7	224	433
24	196	145	342	181	292	160	52.2	53.8	25.8	38.6	208	429
25	243	291	329	203	285	149	51.5	51.1	26.4	35.8	190	384
26	258	471	342	270	293	144	50.3	42.5	27	36.9	172	510
27	427	356	364	292	280	158	48.7	41.2	28.5	106	158	515
28	838	420	354	359	286	152	47.6	39.6	29.3	120	146	673
29	903	594	310	387	303	136	50.8	37.3	28.2	124	136	771
30	830	---	275	353	303	134	58.7	35.6	29.6	99.6	128	577
31	806	---	249	---	276	---	52.4	34.3	---	84.1	---	447
TOTAL	8701	8615	8657	8389	10213	---	2284	1265	894	1357	6394	8986
MEAN	281	297	279	280	329	---	74	41	30	44	213	290
MAX	903	748	474	434	493	---	126	54	33	124	486	771
MIN	129	145	169	179	233	---	48	34	26	23	109	91
AC-FT	16899	16732	16813	16293	19835	---	4435	2457	1736	2635	12418	17452

Table 8.7												
SEATTLE PUBLIC UTILITIES												
Data Retrieved from SPU IMS SCADA Database: 2022-03-03												
LANDSBURG TUNNEL - FLOW VOL 24 HR TOT - MG												
SOURCE AGENCY SPU IMS												
LATITUDE 472247 LONGITUDE 1215856 NAD27 DRAINAGE AREA 124 sq. mi. DATUM 490 NGVD29												
All Data is Provisional and Subject to Revision												
Flow Volume, Million Gallons												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
24 Hour Total												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	65	116	66	49	74	66	127	100	96	88	67	70
2	65	86	60	54	68	59	128	107	103	83	63	64
3	75	70	48	63	71	6	127	111	111	86	63	65
4	74	69	46	66	67	97	122	107	111	73	63	67
5	75	83	46	74	68	137	105	111	109	68	68	64
6	82	89	46	69	69	84	86	116	110	68	79	64
7	91	91	47	74	67	66	87	128	114	70	49	76
8	91	86	47	73	72	4	86	133	124	76	36	87
9	45	91	56	95	65	0	106	116	116	94	42	82
10	75	88	66	106	72	0	120	111	119	83	42	58
11	90	91	65	105	74	0	124	112	94	94	42	52
12	82	98	67	92	67	0	128	95	77	81	41	61
13	80	85	64	79	68	0	125	94	90	88	42	59
14	80	68	69	77	68	0	124	94	101	83	43	51
15	76	72	63	76	77	32	122	110	95	78	43	49
16	78	57	62	74	71	128	124	120	84	74	42	59
17	88	57	60	77	75	139	121	126	94	72	27	85
18	95	67	65	74	75	132	114	124	89	85	24	74
19	96	71	71	72	74	136	113	117	91	87	46	56
20	95	70	71	67	79	131	112	108	89	81	50	49
21	95	71	104	64	87	127	105	106	88	81	52	51
22	95	71	114	62	89	123	80	93	92	81	58	52
23	87	74	110	60	94	122	101	95	81	60	58	51
24	79	73	114	58	104	120	108	1	87	54	58	50
25	79	76	112	80	92	113	106	78	82	51	63	51
26	81	73	88	86	91	117	111	95	82	55	66	23
27	42	75	88	89	92	127	115	102	81	40	74	0
28	0	73	55	88	90	120	116	107	78	51	74	27
29	82	69.6	51	84	92	112	110	108	0	55	76	48
30	127	---	51	88	114	118	102	106	79	58	72	50
31	115	---	49	63.1	146	---	97	108	---	57	---	48.5
TOTAL	2477	2257	2121	2333	2511	2416	3451	3234	2766	2256	1622	1741
MEAN	79	78	68	75	81	81	111	104	92	73	54	56
MAX	127	116	114	106	146	139	128	133	124	94	79	87
MIN	0	57	46	49	65	0	80	1	0	40	24	0

Table 8.8												
SEATTLE PUBLIC UTILITIES												
Data Retrieved from SPU IMS SCADA Database: 2022-03-03												
LANDSBURG WEATHER STATION - PRECIP 24HR TOT ODE												
SOURCE AGENCY SPU IMS												
LATITUDE 472247 LONGITUDE 1215856 NAD27 DATUM 490 NGVD29												
All Data is Provisional and Subject to Revision												
Rainfall, Inches												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
24 Hour Total												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	0	0.14	0.11	0.21	0	0.04	0.01	0.11	0.23	0.02	0.02	0.37
2	0.03	0.22	0.14	0.01	0.03	0.1	0	0	0.01	0	0.01	0
3	0	0.09	0	0.04	0.21	0.03	0.25	0.08	0.13	0.2	0.02	0.21
4	0.15	0.16	0.02	0	0.02	0.01	0	0	0.04	0.02	0	0.13
5	0.19	0.26	0	0.02	0.03	0.24	0.22	0.28	0.21	0.35	0.05	0
6	0.05	0	0.14	0	0	0.04	0.06	0.15	0	0.01	0.72	0.59
7	0.68	0.01	0	0.05	0.17	0.26	0	0.01	0.04	0.24	0	0.42
8	0.03	0.05	0.13	0.02	0	0.02	0.37	0	0	0.45	0.06	0.25
9	0.02	0	0.1	0.26	0.07	0	0.27	0.09	0.19	0.01	0.08	0.62
10	0.05	0.18	0.08	0	0.06	0.05	0.59	0	0.02	0	0	0.02
11	0.16	0.11	0.17	0.13	0	0.02	0.03	0.07	0	0.27	0.02	0.12
12	0.27	0.02	0	0.05	0.04	0	0.05	0	0.43	0.16	0.62	0.54
13	0.01	0.3	0.02	0	0	0.01	0.25	0.02	0.3	0.3	0.03	0.03
14	0.04	0.1	0	0.07	0.08	0.2	0	0.16	0.38	0.04	0.07	0.16
15	0	0.05	0.13	0.03	0	0.15	0.01	0.01	0.02	0.06	0.12	0.08
16	0.12	0	0.04	0.13	0.08	0.12	0	0.1	0.03	0.34	0	0.07
17	0.26	0.36	0.03	0.14	0	0.03	0.02	0.2	0.09	0	0.01	0.3
18	0.59	0.03	0.01	0	0.13	0.1	0.07	0	0	0.06	0.28	0.01
19	0	0.4	0.14	0.15	0.14	0	0.18	0.01	0.01	0	0	0.21
20	0.03	0.08	0.06	0	0	0.23	0	0	0	0.07	0.26	0
21	0	0	0	0.02	0.04	0.16	0.03	0.02	0.29	0.17	0.25	0.028
22	0.02	0.01	0.14	0	0	0.02	0.04	0.07	0	0	0.5	0.033
23	0	0	0.24	0.04	0.01	0	0	0	0.03	0.01	0.2	0
24	0.1	0.15	0	0.15	0	0.52	0.08	0.06	0	0	0	0.37
25	0.12	0	0.01	0	0.04	0.32	0.11	0	0.08	0.21	0.01	0.31
26	0.37	0.11	0.06	0.21	0	0	0	0.08	0	0.04	0.08	0
27	0.01	0.01	0	0	0.02	0.11	0.11	0	0.09	0.03	0	0.21
28	0.09	0.1	0.1	0.03	0.07	0.08	0.07	0.44	0.34	0.3	0.23	0.1
29	0.11	0	0.07	0.01	0.05	0	0	0	0.42	0.16	0	0.13
30	0	---	0.02	0.17	0.13	0.18	0.002	0.65	0.15	0.11	0.05	0
31	0.1	---	0.36	0.37	0.11	---	0.23	0.38	---	0	---	0.59
TOTAL	3.6	2.9	2.3	2.3	1.5	3.0	3.1	3.0	3.5	3.6	3.7	5.9
MEAN	0.1	0.1	0.1	0.1	0.0	0.1	0.1	0.1	0.1	0.1	0.1	0.2
MAX	0.68	0.40	0.36	0.37	0.21	0.52	0.59	0.65	0.43	0.45	0.72	0.62
MIN	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Table 8.9												
SEATTLE PUBLIC UTILITIES												
Data Retrieved from SPU IMS SCADA Database: 2021-03-03												
MASONRY WEATHER STATION - PRECIP 24HR TOT ODE												
SOURCE AGENCY SPU IWRMS												
LATITUDE 472443 LONGITUDE 1214504 NAD27 DATUM 490 NGVD29												
All Data is Provisional and Subject to Revision												
Rainfall, Inches												
CALENDAR YEAR JANUARY TO DECEMBER 2024												
24 Hour Total												
DAY	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	0	0.06	0.11	0.35	0	0.02	0	1.11	0.62	0.39	0.88	1.14
2	0.07	0	0.5	0.24	0.33	0	0.58	0.2	0.1	0.03	0.77	0.53
3	0.87	0.34	0.35	0	0.72	0.03	0.32	0.01	0.1	0.01	0.1	0.06
4	0.73	0	0.13	0.01	0.29	0	0.11	0.15	0	0	1.42	1.56
5	1.21	1.2	0.65	0.16	0.34	0.16	0.32	0.13	0	0.43	1.11	0.99
6	0.35	0.25	0.41	1.12	0.01	0.17	0.45	0.47	0.16	0.58	0.38	1.42
7	0.12	0	1.09	0.03	0	0	1.02	0.26	0.17	0.32	0.2	0.85
8	1.9	0.01	0.15	0	0.25	0.14	0.01	0.18	0	0.11	0.01	0.62
9	0.23	0	0.02	0.01	0.02	0.75	0.14	0.1	0.14	0.32	0.15	0.6
10	0.17	0.37	0.01	0	0	0.01	0.01	0	0.75	0.45	0.13	0.1
11	0.2	0.61	0	1.03	0.9	0	0.28	0.14	0.01	1.02	0.47	0.1
12	0	0.01	0.68	0.25	0.01	0.14	2.35	0	0	0.01	0.26	0
13	1.48	0	0	0	0.36	0	0.55	1.1	0.14	0.14	0.18	0.04
14	0.22	1.23	0.33	1.59	0.11	0.06	0.76	1.45	0	0.01	0.1	0.29
15	0.07	1.02	0.09	0.17	0.02	0.01	0.1	0	0.06	0.28	0	0.8
16	0.68	0.28	0.38	0	0	0	0.22	0.01	0.01	2.35	0.14	0.22
17	0.78	0.99	0.18	0.36	0.02	0.02	1.29	0	0	0.55	0	0.2
18	0.49	1.88	1.09	0.22	0	0.37	1.09	0.04	0.02	0.76	1.1	2.1
19	0.79	0.12	0.09	0.14	0.89	0.46	0.48	0.29	0.37	0.1	1.45	0.01
20	0.42	0.17	0.01	0	0.37	0.01	0.54	0.8	0.46	0.22	0	0.56
21	0.78	0.52	0.08	1.44	0.01	0.02	0.02	0.2	0.01	1.29	0.01	1.14
22	1.22	0.02	0	0.01	0	0	0.06	2.1	0.02	1.09	0	0.53
23	0.12	0	0.07	0	0.01	0.12	0	0.01	0	0.48	0.04	0.06
24	0	0.18	0.14	0.3	0.35	0	0.22	0.56	0.12	0.54	0.29	1.56
25	0.32	0.77	0	2.46	0.19	0.68	0.74	1.14	0.01	0.02	0.8	0.99
26	0.09	0.34	0.31	0.56	0.01	0.01	1.1	0.53	0	0.06	0.22	1.42
27	0.16	0.01	0	0.75	0.23	0	0.81	0.06	0.68	0	0.2	0.85
28	0.14	0	0.54	0.02	0.89	0.39	0.88	1.56	0.01	0.22	2.1	0.62
29	0.12	0.52	1.6	0	0.38	0.03	0.77	0.99	0	0.74	0.01	0.6
30	0	---	0.73	0.02	0	0.01	0.1	1.42	0.02	1.1	0.56	0.1
31	0.23	---	1.23	---	0.73	---	1.42	0.85	---	0.81	---	0.02
TOTAL	14.0	10.9	11.0	11.2	7.4	3.6	16.7	15.9	4.0	14.4	13.1	20.1
MEAN	0.5	0.4	0.4	0.4	0.2	0.1	0.5	0.5	0.1	0.5	0.4	0.6
MAX	1.9	1.9	1.6	2.5	0.9	0.8	2.4	2.1	0.8	2.4	2.1	2.1
MIN	0	0	0	0	0	0	0	0	0	0	0	0

APPENDIX 1: Guaranteed Instream Flow
Schedule with June 4, 2009 Walsh Ditch
Adjustment, USGS Gage 12117600.

Water Week Starting	Critical Instream Flow Requirement	Normal Instream Flow Requirement	Normal Supplemental Instream Flow Requirement
1-Oct.	103	214	214
8-Oct.	133	279	334
15-Oct.	163	279	334
22-Oct.	183	279	334
29-Oct.	203	279	334
5-Nov.	203	279	334
12-Nov.	203	284	339
19-Nov.	203	284	339
26-Nov.	206	292	347
3-Dec.	206	292	347
10-Dec.	206	292	347
17-Dec.	206	292	347
24-Dec.	206	290	345
31-Dec.	188	275	275
7-Jan.	188	275	275
14-Jan.	188	275	275
21-Jan.	188	275	275
28-Jan.	188	275	275
4-Feb.	188	275	275
11-Feb.	188	273	378
18-Feb.	188	273	378
25-Feb.	188	273	378
4-Mar.	188	273	378
11-Mar.	188	273	378
18-Mar.	188	273	378
25-Mar.	188	273	378
1-Apr.	188	273	378
8-Apr.	186	273	378
15-Apr.	186	273	273
22-Apr.	196	268	268
29-Apr.	196	268	268
6-May	200	268	268
13-May	205	268	268
20-May	215	258	258
27-May	215	258	258
3-Jun.	205	256	256
10-Jun.	205	231	231
*17-Jun.	164	231	246
24-Jun.	104	231	246
1-Jul.	84	174	240
8-Jul.	84	109	209
15-Jul.	84	84	200
22-Jul.	83	84	168
29-Jul.	73	83	119
5-Aug.	73	83	83
12-Aug.	73	83	83
19-Aug.	73	83	83
26-Aug.	73	83	83
2-Sept.	73	83	83
9-Sept.	72	83	83
16-Sept.	82	98	136
23-Sept.	82	98	213

*From June 17 through August 4, actual annual supplemental flow levels will vary according to daily allocations established by Cedar River Instream Flow Commission